

Quantifizierung Wärmebrücken

Fenster- und Fensteranschluss

Leitdetails für typische Fenstersanierungslösungen unter Angabe der Wärmedurchgangskoeffizienten und der Psi-Werte.

Analyse des hygrothermischen Risikos an kritischen Punkten

Am Beispiel eines neuen Einfachfensters mit Isolierverglasung eingebaut in eine historische Natursteinmauer

Optimierung am Glasabstandshalter

Fensterrahmen unten	Abstandshalter 1	Abstandshalter 2	Abstandshalter 3
Simulation Fenster mit 3 verschiedenen Lösungen für den Glas-Abstandshalter			
Beschreibung	Warm-Edge-Edelstahl- Abstandhalter mit 6,5mm und einer Wandstärke von 0,18 mm (Chromatech)	7 mm hoher Warm- Edge-Edelstahl- Abstandhalter mit 0,15 mm Wandstärke mit geriffelter Oberfläche zur Lichtbrechung (Chromatech Plus)	Reduzierte Profilhöhe: 6,9 mm; niedriger Wärmedurchlass: Edelstahl 15,0 W/(mK), Spezialkunststoff 0,17 W/(mK) (Chromatech Ultra)
f_{Rsi}	0.583	0.593	0.640
T_{min}	11.3°C	11.5°C	12.5°C
U_f in W/m²K;	1.55	1.55	1.55
ψ_g in W/mK	0.063	0.060	0.0458

*bei Außentemperatur von -0.9 und rel. Feuchte innen 42.5%

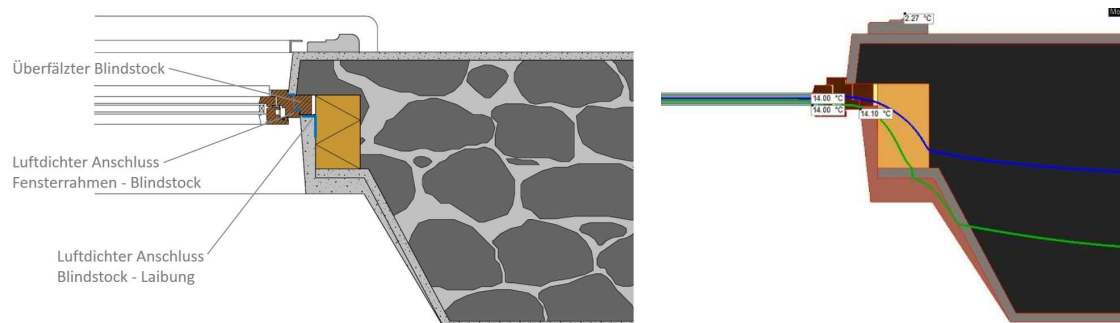
Detail Glasabstandhalter: Die thermische Simulation des unteren Profils des für einen Fensteraustausch vorgeschlagenen Fensters ergibt einen Wärmebrückenkoeffizienten der Verglasungskante, ψ_g , von 0,063 W/mK und einen Kondensationstemperaturfaktor, f_{Rsi} , von 0,583. Letzterer erfüllt nicht die Anforderungen des Casaclima R-Protokolls. Es wird vorgeschlagen den ursprünglich vorgesehenen Abstandhalter aus Edelstahl (1) mit einem Abstandhalter aus Edelstahl mit optimierter Geometrie (2) oder mit einem Hybrid-Abstandhalter aus Spezialkunststoff und einer feinen Struktur aus Edelstahl (3) zu ersetzen. Wie in Abbildung dargestellt, verursachen diese Abstandhalter keine hygrothermischen Risiken und führen zu einer Verbesserung der Wärmebrücke.

Optimierung Fenster-Wand-Anschluss

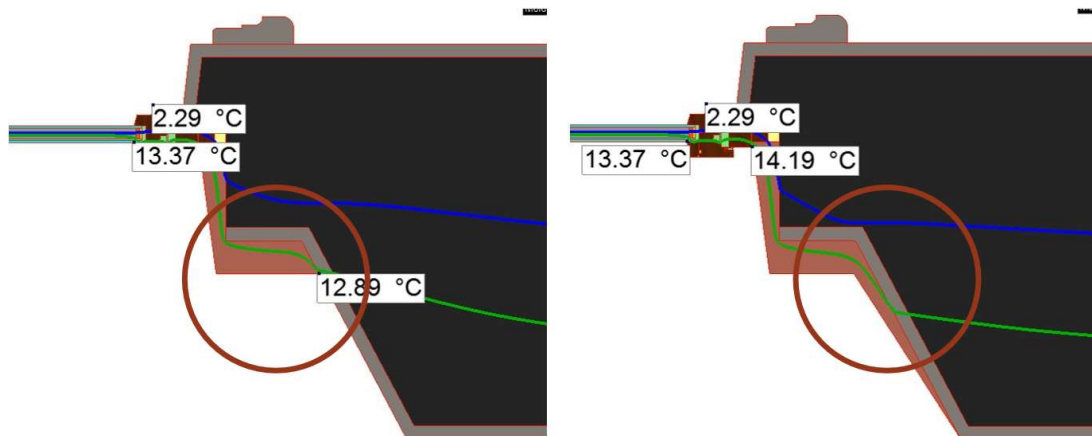
Horizontalanschluss seitlich Fenster-Natursteinmauer			
Detail	Bestehender Fenster-Wand-Anschluss	Verbesserung	Weitere Verbesserung
Horizontal-anschluss Fenster-Wand			
Maßnahme	Austausch Fenster, ohne weitere Maßnahmen	+ 4 cm Dämmputz λ 0,057 W/mK + 0-2 cm keilförmig in der Laibung	+ Dämmung im Hohlraum λ 0,043 seitlich hinter dem bestehenden Putz
T_{min}	12.5°C (< 12.6°C)	14.2 (> 12.6°C)	14.6 (> 12.6°C)
f_{Rsi}	0.580 (< 0.587)	0.629 (> 0.587)	0.630 (> 0.587)
Ergebnis	Anforderungen nicht erfüllt. Gefahr von Tauwasser-/Schimmelbildung*	Anforderungen erfüllt. Keine Gefahr von Tauwasser-/Schimmelbildung*	Anforderungen erfüllt. Keine Gefahr von Tauwasser-/Schimmelbildung*

* siehe Schimmelisotherm in grün bei 12,6°C; gemäß Klimahaus Anforderungen

Detail der horizontalen Fenster-Wand-Verbindung: In der Abbildung werden drei Ausführungsvarianten für den Fenster-Wandanschluss nach dem Fensteraustausch dargestellt. Sie zeigt, dass ein Austausch des Fensters ohne weitere Maßnahmen an der Laibung, aus hygrothermischer Sicht nicht zu empfehlen ist. Es wird vorgeschlagen, (i) die Brüstung und die Laibungen mit mindestens vier cm Dämmputz (λ 0,057 W/mK) zu dämmen und (ii) eine flexible Dämmung in dem Hohlraum, hinter dem vorhandenen Putz seitlich und unterhalb des Fensters (der nach dem Entfernen des alten Fensters zum Vorschein gekommen ist) hinzuzufügen.



Darüber hinaus empfehlen wir, die Luftdichtheit am Fenster-Blindstock-Wandanschluss zu verbessern und den Dämmputz keilförmig auslaufen zu lassen, um hygrothermische Risiken am Übergangspunkt zu vermeiden.



Unterer Anschluss - Parapet, Fenster mit Chromatherm

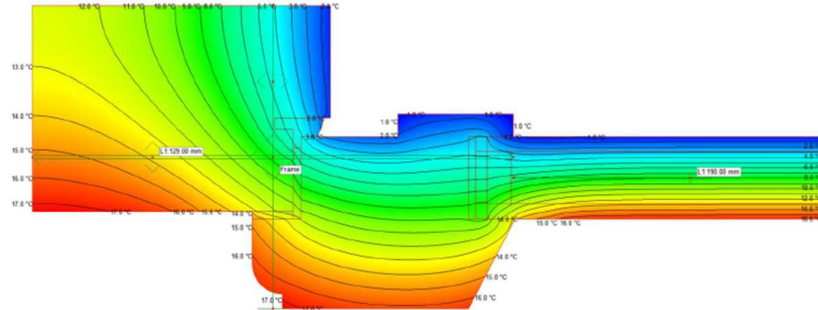
Detail	Vertikalanschluss unten Fenster-Natursteinmauer		
	Bestand	Verbesserung	Weitere Verbesserung
Horizontal-anschluss Fenster-Wand			
Maßnahme	Austausch Fenster, ohne weitere Maßnahmen	+ 4 cm Dämmputz λ 0,057 W/mK auf der Brüstung + 2 cm horizontal	+ 4 cm Dämmputz λ 0,057 W/mK auf der Brüstung + 2 cm horizontal + Dämmung λ 0,043 W/mK in Hohlraum horizontal
T_{min}	13.2 (> 12.6°C)	13.2 (> 12.6°C)	13.9 (> 12.6°C)
f_{Rsi}	0.589 (> 0.587)	0.618 (> 0.587)	0.618 (> 0.587)
ψ in W/mK	1.5931	0.7208	0.7691
Ergebnis	Anforderungen knapp erfüllt. Gefahr von Tauwasser-/Schimmelbildung*	Anforderungen erfüllt. Keine Gefahr von Tauwasser-/Schimmelbildung*	Anforderungen erfüllt. Keine Gefahr von Tauwasser-/Schimmelbildung*
	✓	✓	✓

* siehe Schimmelisotherm in grün bei 12,6°C; gemäß Klimahaus Anforderungen

Detail der vertikalen Fenster-Wand-Verbindung (unten): In der Abbildung werden ebenfalls drei Ausführungsvarianten für den Fenster-Wandanschluss nach dem Fensteraustausch dargestellt. Ohne weitere Maßnahmen an der Brüstung werden die Anforderungen (unter Standardbedingungen) knapp erfüllt. Eine aus hygrothermischer Sicht sicherere Lösung ist die innenseitige Dämmung der Brüstung mit vier cm Dämmputz (λ 0,057 W/mK) (+ 2 cm horizontal) oder, wenn vorhanden, zusätzlich den entstandenen Hohlraum zu dämmen.

Werte für typische Kastenfenster saniert mit Isolierverglasung (innere Fensterebene)

Frame Uf computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 1.64 W/m²K	- - -
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Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Box 2	0.6100	0.900	
EPDM	0.2500	0.900	
Larch	0.1300	0.900	
Argon	1.0512	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \frac{1}{\frac{1}{U_{f,2D}} + \frac{1}{U_{f,1D}}}$$

$$U_f = \frac{1}{\frac{1}{15.0961 \text{ W/m}^2\text{K}} + \frac{1}{2.7247 \text{ W/m}^2\text{K} \times 0.1900 \text{ m}} + \frac{1}{0.1290 \text{ m}}}$$

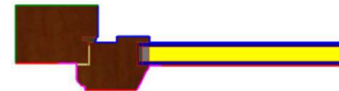
Simulation with ISO10077 panel

Uf2D, with ISO10077 panel:	0.7548 W/mK
Φf, flow with ISO10077 panel:	15.0961 W/m
Flow error:	0.000001
Triangles:	4110

Frame width Bf: 129.00 mm Panel width Bp: 190.00 mm

Boundary conditions

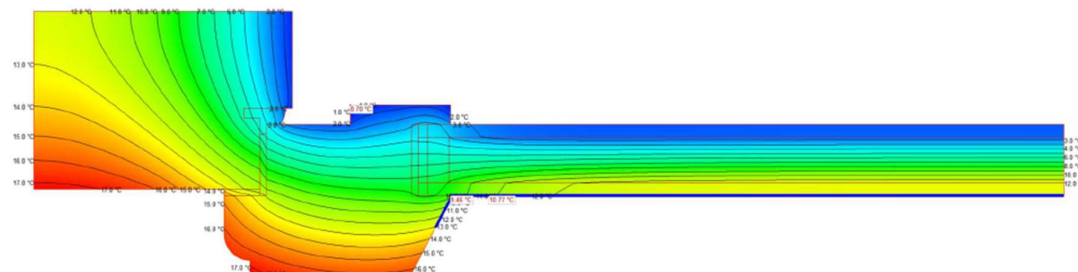
Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000



Project:	Apartment Troi	Detail:	Rahmen l,r,o,b innen	File:	Rahmen l,r,o,u innen
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: 0.025 W/mK Superficial condensation: 221 mm	- - -
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ψ computation

$$\psi = \frac{1}{\frac{1}{U_{f,2D}} + \frac{1}{U_{f,1D}}}$$

$$\psi = \frac{1}{\frac{1}{15.0961 \text{ W/m}^2\text{K}} + \frac{1}{2.7247 \text{ W/m}^2\text{K} \times 0.1900 \text{ m}} + \frac{1}{0.1290 \text{ m}}}$$

Simulation with glazing

Uf2D, with glazing:	0.7548 W/mK
Φf, flow with glazing:	15.0961 W/m
Flow error:	0.000001
Triangles:	4110

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Glazing transmittance Ug=2.72 W/m²K Frame transmittance Uf=1.64 W/m²K

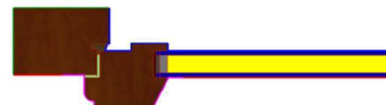
Glazing size Bg: 190 mm

Frame size Bf: 129 mm

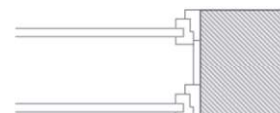
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	269.00	10.768	17.366	13.954	12.5096
External	262.16	0.697	3.582	2.067	-15.0961
Adiabatic	157.00	1.344	17.333	10.504	0.0029
Rsi increased	87.51	9.458	17.366	14.088	2.5865

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Box 2	0.6100	0.900	
EPDM	0.2500	0.900	
Larch	0.1300	0.900	
Argon	1.0512	0.900	
10077 radiosity	-	0.900	



Project:	Apartment Troi	Detail:	Rahmen l,r,o,b innen	File:	Rahmen l,r,o,u innen
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf transmittance computation ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.92 W/m²K

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_{f1}/\Delta T) - \sum (U_{f1}B_p)}{B_f}$$

$$U_f = \frac{([25.2420 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.7244 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}] - [2.7244 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}])}{0.0920 \text{ m}}$$

Simulation with ISO10077 panel

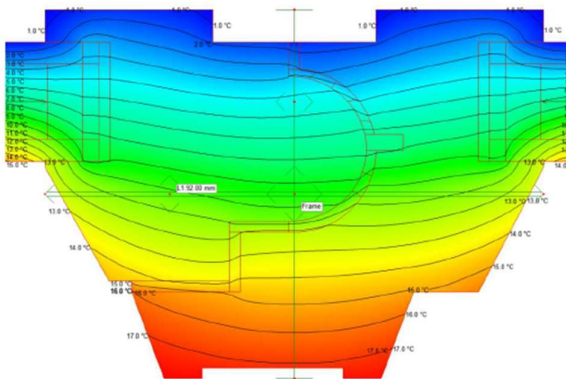
Lf2D, with panel ISO10077:	1.2621 W/mK
Φf, flow with panel ISO10077:	25.2420 W/m
Flow error:	0.000002
Triangles:	7757

Boundary conditions

Name	Col	Air T [°C]	R [m²K/W]
Internal	20.000	0.1300	
External	0.000	0.0400	
Adiabatic	-	-	
Rsi increased	20.000	0.2000	
Rs internal cavities	20.000	0.3000	

Materials

Material	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
EPDM	0.2500	0.900	
Larch	0.1300	0.900	
Argon	1.0512	0.900	
Argon	1.0512	0.900	
10077 radiosity	-	0.900	



Frame length Bf: 92.00 mm Panel length Bp: 380.00 mm

Project:	Apartment Troi	Detail:	Stulp innen	File:	-
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.050 W/mK

Superficial condensation: 446 mm

ψ computation

$$\psi = \frac{(\Phi_{\psi}/\Delta T) - \sum (U_{\psi}B_p)}{B_p}$$

$$\psi = \frac{([25.2420 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.9243 \text{ W/m}^2 \cdot \text{K} \cdot 0.0920 \text{ m}] - [2.7244 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}])}{0.1900 \text{ m}}$$

Glazing transmittance Ug=2.72 W/m²K Frame transmittance Uf=1.92 W/m²K
Glazing size Bg: 380 mm Frame size Bf: 92 mm

Boundary table

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	395.84	10.476	17.873	13.034	21.2115
External	496.00	0.600	3.474	2.036	-25.2420
Adiabatic	44.00	2.175	12.905	7.538	-0.0000
Rsi increased	126.38	9.229	17.873	13.797	3.9201
Rs internal cavities	6.16	14.200	15.943	14.623	0.1104

Simulation with glazing

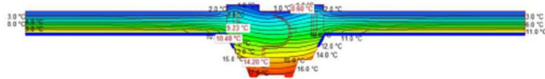
Lp2D, with glazing:	1.2621 W/mK
Φp, flow with glazing:	25.2420 W/m
Flow error:	0.000002
Triangles:	7757

Boundary conditions

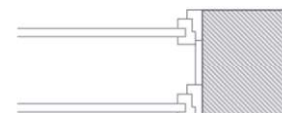
ID	Name	Col	Air T [°C]	R [m²K/W]	H [%]
0	Internal	20.000	0.1300		65.0
1	External	0.000	0.0400		65.0
2	Adiabatic	-	-		65.0
3	Rsi increased	20.000	0.2000		65.0
4	Rs internal cavities	20.000	0.3000		65.0

Materials

Material	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
EPDM	0.2500	0.900	
Larch	0.1300	0.900	
Argon	1.0512	0.900	
Argon	1.0512	0.900	
10077 radiosity	-	0.900	



Project:	Apartment Troi	Detail:	Stulp innen	File:	-
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf transmittance computation ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.60 W/m²K

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum (U_{x,Bp}) / B_f}{B_f}$$

$$U_f = \frac{([25.1538 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.6818 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}] - [-x])}{0.1210 \text{ m}}$$

Simulation with ISO10077 panel

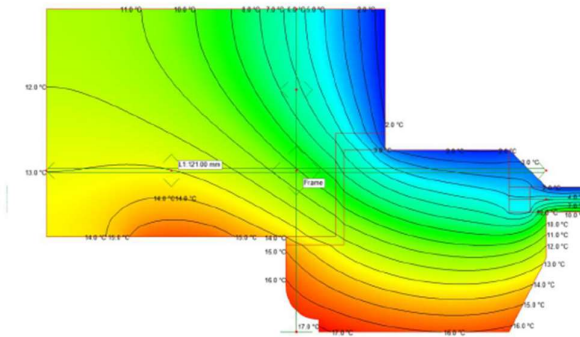
Lf2D, with panel ISO10077:	1.2577 W/mK
Φf, flow with panel ISO10077:	25.1538 W/m
Flow error:	0.000000
Triangles:	2432

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal	20.000	0.1300	
External	0.000	0.0400	
Adiabatic	-	-	
Rsi increased	20.000	0.2000	

Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Larch	0.1300	0.900	
Air	0.0673	0.900	
Putty	0.5000	0.900	



Frame length Bf: 121.00 mm Panel length Bp: 190.00 mm

Project:	Apartment Troi	Detail:	Rahmen I,r,o aussen	File:	-
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.016 W/mK
Superficial condensation: 235 mm

ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - \sum (U_{x,Bg})}{B_g}$$

$$\psi = \frac{([25.1538 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.6015 \text{ W/m}^2 \cdot \text{K} \cdot 0.1210 \text{ m}] - [5.6818 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}])}{-x}$$

Glazing transmittance Ug=5.68 W/m²K Frame transmittance Uf=1.60 W/m²K
Glazing size Bg: 190 mm Frame size Bf: 121 mm

Boundary table

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	239.00	4.679	17.210	8.319	21.4749
External	266.73	1.367	4.545	3.772	-25.1538
Adiabatic	163.00	1.367	14.953	10.314	0.0372
Rsi increased	93.69	4.461	17.210	12.147	3.6769

Simulation with glazing

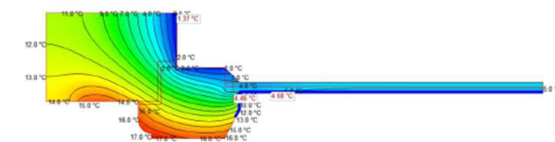
Lp2D, with glazing:	1.2577 W/mK
Φp, flow with glazing:	25.1538 W/m
Flow error:	0.000000
Triangles:	2432

Boundary conditions

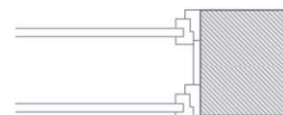
ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal	20.000	0.1300	65.0	
1	External	0.000	0.0400	65.0	
2	Adiabatic	-	-	65.0	
3	Rsi increased	20.000	0.2000	65.0	

Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Larch	0.1300	0.900	
Air	0.0673	0.900	
Putty	0.5000	0.900	



Project:	Apartment Troi	Detail:	Rahmen I,r,o aussen	File:	-
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf transmittance computation

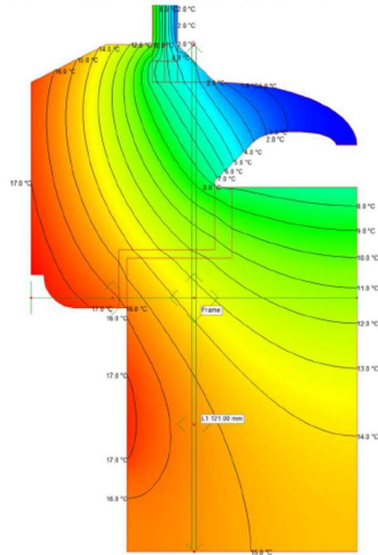
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.19 W/m²K

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum (U_{k,Bp}) / B_f}{\Delta T}$$

$$U_f = \frac{[23.5193 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.4945 \text{ W/m}^2 \times 0.1900 \text{ m}] - [x]}{0.1210 \text{ m}}$$



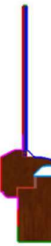
Simulation with ISO10077 panel

Lf2D, with panel ISO10077:	1.1760 W/mK
Φf, flow with panel ISO10077:	23.5193 W/m
Flow error:	0.000006
Triangles:	2678

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal	20.000	0.1300	
External	0.000	0.0400	
Adiabatic			
Rsi increased	20.000	0.2000	
Rs external cavities	0.000	0.3000	

Name	λx [W/mK]	ε	Color
Air	0.0735	0.900	
Larch	0.1300	0.900	
Putty	0.5000	0.900	
Glass	0.5000	0.900	



Frame length Bf: 121.00 mm Panel length Bp: 190.00 mm

Project:	Apartment Troi	Detail:	Rahmen u aussen	File:	-
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation

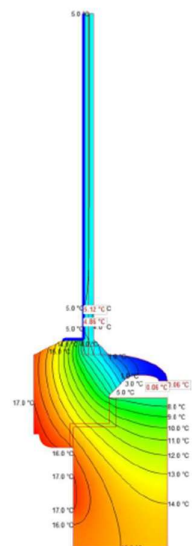
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.012 W/mK
Superficial condensation: 227 mm

ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - \sum (U_{k,Bp}) / B_{\psi}}{\Delta T}$$

$$\psi = \frac{[23.5193 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.1929 \text{ W/m}^2 \times 0.1210 \text{ m}] - [5.4945 \text{ W/m}^2 \times 0.1900 \text{ m}]}{-0.012}$$



Glazing transmittance Ug=5.49 W/m²K Frame transmittance Uf=1.19 W/m²K
Glazing size Bg: 190 mm Frame size Bf: 121 mm

Boundary table

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	239.00	5.119	17.926	8.959	20.2980
External	242.65	0.062	4.396	3.685	-22.3560
Adiabatic	168.00	4.396	16.697	13.333	0.0198
Rsi increased	93.69	4.861	17.926	13.123	3.2214
Rs external cavities	74.88	0.062	8.008	4.660	-1.1632

Simulation with glazing

Lp2D, with glazing:	1.1760 W/mK
Φp, flow with glazing:	23.5193 W/m
Flow error:	0.000006
Triangles:	2678

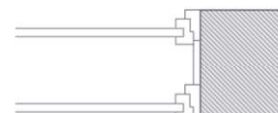
Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal	20.000	0.1300		65.0
1	External	0.000	0.0400		65.0
2	Adiabatic				65.0
3	Rsi increased	20.000	0.2000		65.0
5	Rs external cavities	0.000	0.3000		65.0

Name	λx [W/mK]	ε	Color
Air	0.0735	0.900	
Larch	0.1300	0.900	
Putty	0.5000	0.900	
Glass	0.5000	0.900	

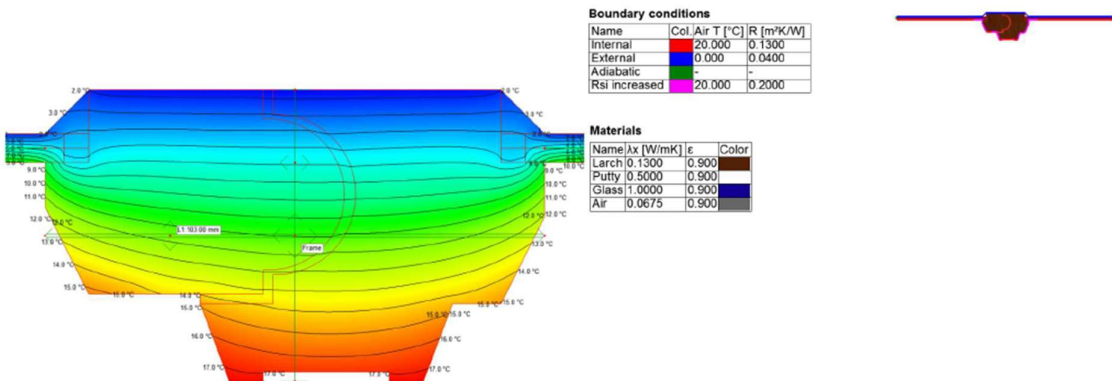


Project:	Apartment Troi	Detail:	Rahmen u aussen	File:	-
Client:	-	Date:	28/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf transmittance computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 2.28 W/m²K
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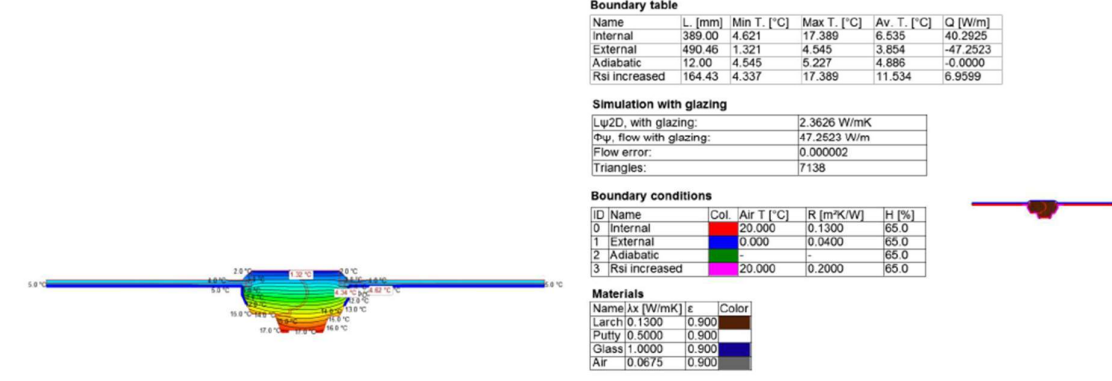
Frame Uf transmittance computation $U_f = \frac{(\Phi_f / \Delta T) - \sum [U_{x,Bp}] / B_f}{B_f}$ $U_f = \frac{([47.2523 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.6818 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [5.6818 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]) / 0.1030 \text{ m}}$	Simulation with ISO10077 panel Lf2D, with panel ISO10077: 2.3626 W/mK Φf, flow with panel ISO10077: 47.2523 W/m Flow error: 0.000002 Triangles: 7138
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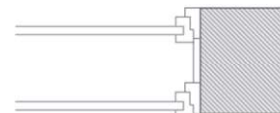
Project: Apartment Troi Client: -	Detail: Stulp aussen Date: 28/09/2019	File: - Software: Frame Simulator - 4.0.5 b839 64bit
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ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: -0.031 W/mK Superficial condensation: 478 mm
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ψ computation $\psi = \frac{(\Phi_\psi / \Delta T) - \sum [U_{x,Bg}]}{B_g}$ $\psi = \frac{([47.2523 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.2751 \text{ W/m}^2 \text{K} \times 0.1030 \text{ m}] - [5.6818 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [5.6818 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}])}{0.1030 \text{ m}}$	Glazing transmittance Ug=5.68 W/m²K Glazing size Bg: 380 mm Frame transmittance Uf=2.28 W/m²K Frame size Bf: 103 mm
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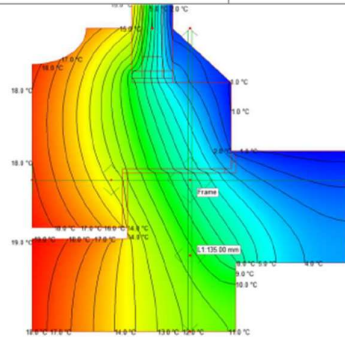


Project: Apartment Troi Client: -	Detail: Stulp aussen Date: 28/09/2019	File: - Software: Frame Simulator - 4.0.5 b839 64bit
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Neues Kastenfenster

Frame Uf computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 1.22 W/m²K
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Materials

Name	λ_x [W/mK]	ϵ	Color
Larch	0.1300	0.900	
EPDM	0.2500	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
Putty	0.5000	0.900	
Cripto	0.0458	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \frac{1}{\frac{1}{\Phi_f / \Delta T} + \sum \frac{U_{x,Bp}}{B_f}}$$

$$U_f = \frac{1}{\frac{1}{14.0415 \text{ W/m}^2 \cdot \text{K}} + \frac{2.6617 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}}{0.1350 \text{ m}}}$$

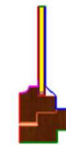
Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	0.7021 W/mK
Φ_f , flow with ISO10077 panel:	14.0415 W/m
Flow error:	0.000008
Triangles:	4066

Frame width Bf: 135.00 mm Panel width Bp: 190.00 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000
Rs internal cavities		20.000	0.3000

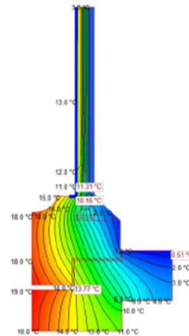


Project:	Aerztehaus Ried	Detail:	Rahmen n o,u,l,r innen	File:	Rahmen innen o,u,l,r
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Simulator

ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: 0.032 W/mK Superficial condensation: 214 mm
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ψ computation

$$\psi = \frac{1}{\frac{1}{\Phi_\psi / \Delta T} + \sum \frac{U_{g,Bf}}{B_\psi}}$$

$$\psi = \frac{1}{\frac{1}{14.0415 \text{ W/m}^2 \cdot \text{K}} + \frac{2.6617 \text{ W/m}^2 \cdot \text{K} \cdot 0.1350 \text{ m}}{0.1900 \text{ m}}}$$

Simulation with glazing

Lp2D, with glazing:	0.7021 W/mK
Φ_ψ , flow with glazing:	14.0415 W/m
Flow error:	0.000008
Triangles:	4066

Boundary conditions

ID/Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0 Internal		20.000	0.1300	65.0
1 External		0.000	0.0400	65.0
2 Adiabatic		-	-	65.0
3 Rsi increased		20.000	0.2000	65.0
4 Rs internal cavities		20.000	0.3000	65.0

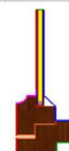
Materials

Name	λ_x [W/mK]	ϵ	Color
Larch	0.1300	0.900	
EPDM	0.2500	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
Putty	0.5000	0.900	
Cripto	0.0458	0.900	
10077 radiosity	-	0.900	

Glazing transmittance $U_g=2.66 \text{ W/m}^2\text{K}$ Frame transmittance $U_f=1.22 \text{ W/m}^2\text{K}$
 Glazing size Bg: 190 mm Frame size Bf: 135 mm

Boundary temperatures

Name	L [mm]	Min T. [°C]	Max T. [°C]	Av. T. [°C]	Q [W/m]
Internal	290.00	11.308	19.030	14.955	11.2541
External	307.95	0.512	2.891	1.824	-14.0415
Adiabatic	239.42	0.512	18.555	8.774	-0.0287
Rsi increased	66.09	10.165	18.207	14.542	1.8696
Rs internal cavities	89.67	13.765	19.030	16.929	0.9178

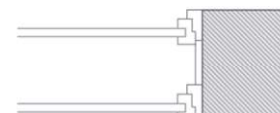


Project:	Aerztehaus Ried	Detail:	Rahmen n o,u,l,r innen	File:	Rahmen innen o,u,l,r
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



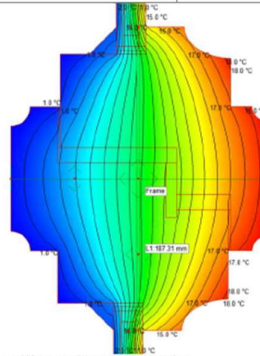
Frame Simulator

Kastenfenster



Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.22 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Cripto	0.0458	0.900	
Cripto	0.0458	0.900	
Larch	0.1300	0.900	
EPDM	0.2500	0.900	
Putty	1.0000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum (U_{x,Bp}) / B_f}{B_f}$$

$$U_f = \frac{([26.4885 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.6614 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [2.6613 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]) / 0.1873 \text{ m}}$$

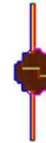
Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	1.3244 W/mK
Φf, flow with ISO10077 panel:	26.4885 W/m
Flow error:	0.000004
Triangles:	6563

Frame width Bf: 187.31 mm Panel width Bp: 380.00 mm

Boundary conditions

Name	Col	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000



Project: Aertzehaus Ried

Detail: Setzholz innen

File: Setzholz innen

Client: -

Date: 16/09/2019

Software: Frame Simulator - 4.0.5 b839 64bit

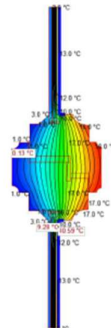


Frame Simulator

ψ and condensation computation
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.085 W/mK

Superficial condensation: 428 mm



ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - [U_f \times B_f] - \sum [U_{g,Bg}]}{B_{\psi}}$$

$$\psi = \frac{[26.4885 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.2183 \text{ W/m}^2 \text{K} \times 0.1873 \text{ m}] - [2.6614 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [2.6613 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]}{0.1873 \text{ m}}$$

Glazing transmittance Ug=2.66 W/m²K

Frame transmittance Uf=1.22 W/m²K

Glazing size Bg: 380 mm

Frame size Bf: 187 mm

Simulation with glazing

Lp2D, with glazing:	1.3244 W/mK
Φψ, flow with glazing:	26.4885 W/m
Flow error:	0.000004
Triangles:	6563

Boundary conditions

ID	Name	Col	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	462.43	10.591	18.778	13.968	21.4577
External	666.43	0.131	3.214	1.590	-26.4885
Adiabatic	36.33	2.126	13.073	7.599	-0.0000
Rsi increased	228.11	9.279	18.778	15.589	5.0307

Materials

Name	λx [W/mK]	ε	Color
Cripto	0.0458	0.900	
Cripto	0.0458	0.900	
Larch	0.1300	0.900	
EPDM	0.2500	0.900	
Putty	1.0000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	

Name	λx [W/mK]	ε	Color
10077 radiosity	-	0.900	



Project: Aertzehaus Ried

Detail: Setzholz innen

File: Setzholz innen

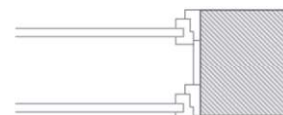
Client: -

Date: 16/09/2019

Software: Frame Simulator - 4.0.5 b839 64bit

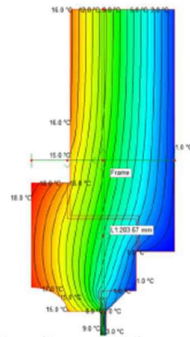


Frame Simulator



Frame Uf computation ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.55 W/m²K



Materials

Name \ x	[W/mK]	ε	Color
Glass	1.0000	0.900	
Putty	0.5000	0.900	
Larch	0.1300	0.900	
Air	0.0826	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum [U_{k,Bp}] / B_f}{\Delta T}$$

$$U_f = \frac{([28.1301 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.7471 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [-x]) / 0.2037 \text{ m}}$$

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	1.4065 W/mK
Φf, flow with ISO10077 panel:	28.1301 W/m
Flow error:	0.000004
Triangles:	1878

Frame width Bf: 203.67 mm Panel width Bp: 190.00 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000

Project: Aertzehaus Ried
Client: -

Detail: Rahmen horizontal aussen o,l,r
Date: 16/09/2019

File: Schnitt horizontal aussen o,l,r
Software: Frame Simulator - 4.0.5 b839 64bit

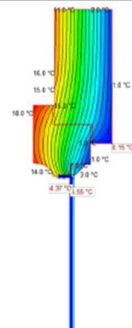


Frame Simulator

ψ and condensation computation ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.001 W/mK

Superficial condensation: 224 mm



ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - [U_f \times B_f]}{\Delta T} - \sum [U_{g \times B_g}]$$

$$\psi = \frac{([28.1301 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.5497 \text{ W/m}^2 \text{K} \times 0.2037 \text{ m}] - [5.7471 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [-x])}{\Delta T}$$

Simulation with glazing

Lp2D, with glazing:	1.4065 W/mK
Φψ, flow with glazing:	28.1301 W/m
Flow error:	0.000004
Triangles:	1878

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Glazing transmittance Ug=5.75 W/m²K Frame transmittance Uf=1.55 W/m²K

Glazing size Bg: 190 mm

Frame size Bf: 204 mm

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	337.50	4.546	18.477	10.635	24.3118
External	431.67	0.148	4.596	2.607	-28.1301
Adiabatic	74.60	1.109	18.309	8.469	-0.0001
Rsi increased	120.40	4.366	18.477	13.657	3.8182

Materials

Name \ x	[W/mK]	ε	Color
Glass	1.0000	0.900	
Putty	0.5000	0.900	
Larch	0.1300	0.900	
Air	0.0826	0.900	

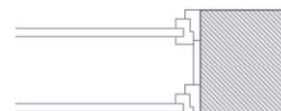
Project: Aertzehaus Ried
Client: -

Detail: Rahmen horizontal aussen o,l,r
Date: 16/09/2019

File: Schnitt horizontal aussen o,l,r
Software: Frame Simulator - 4.0.5 b839 64bit

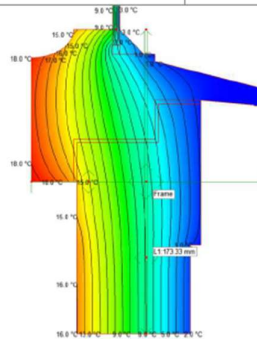


Frame Simulator



Frame Uf computation
 ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.57 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Larch	0.1300	0.900	
Putty	0.5000	0.900	
Glass	1.0000	0.900	
Air	0.1101	0.900	

Frame Uf transmittance computation

$$U_f = ([\Phi_f / \Delta T] - \sum [U_{x,Bp}] / B_f)$$

$$U_f = ([27.2612 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.7471 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] / 0.1733 \text{ m})$$

Frame width Bf: 173.33 mm Panel width Bp: 190.00 mm

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	1.3631 W/mK
Φf, flow with ISO10077 panel:	27.2612 W/m
Flow error:	0.000001
Triangles:	2052

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000



Project:	Aerztehaus Ried	Detail:	Rahmen u aussen	File:	Schnitt vertikal aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit

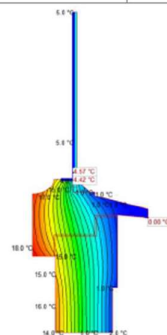


Frame Simulator

ψ and condensation computation
 ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.001 W/mK

Superficial condensation: 224 mm



ψ computation

$$\psi = [\Phi_{\psi} / \Delta T] - [U_f \times B_f] - \sum [U_{g,Bg}]$$

$$\psi = [27.2612 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.5693 \text{ W/m}^2 \text{K} \times 0.1733 \text{ m}] - [5.7471 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]$$

Glazing transmittance Ug=5.75 W/m²K Frame transmittance Uf=1.57 W/m²K
Glazing size Bg: 190 mm Frame size Bf: 173 mm

Simulation with glazing

Lf2D, with glazing:	1.3631 W/mK
Φψ, flow with glazing:	27.2612 W/m
Flow error:	0.000001
Triangles:	2052

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	307.17	4.575	18.498	10.064	23.4774
External	466.29	0.002	4.598	2.339	-27.2613
Adiabatic	68.58	1.189	16.054	8.374	-0.0001
Rsi increased	120.42	4.416	18.498	13.716	3.7838

Name	λx [W/mK]	ε	Color
Larch	0.1300	0.900	
Putty	0.5000	0.900	
Glass	1.0000	0.900	
Air	0.1101	0.900	

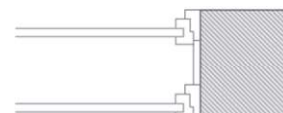


Project:	Aerztehaus Ried	Detail:	Rahmen u aussen	File:	Schnitt vertikal aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



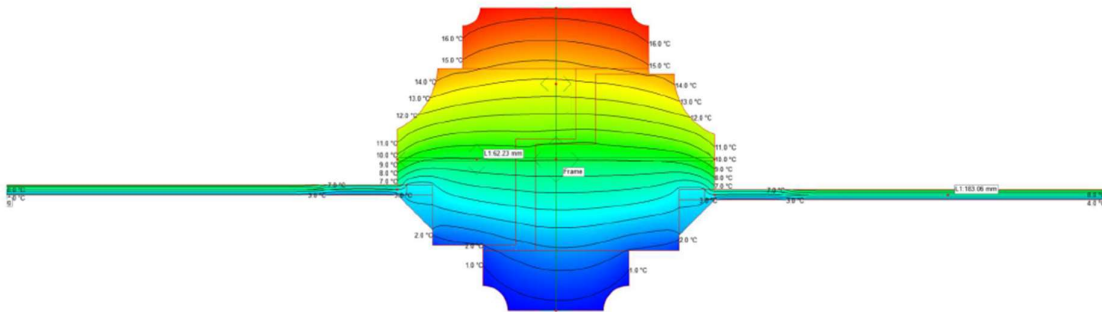
Frame Simulator

Kastenfenster



Frame Uf computation ISO 10077-2 (2017) - radiosity

Transmittance Uf: 2.63 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Putty	1.0000	0.900	
Larch	0.1300	0.900	
Glass	1.0000	0.900	
Air	0.0764	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum (U_{x,Bp})}{B_f}$$

$$U_f = \frac{[45.5536 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.8140 \text{ W/m}^2 \text{K} \times 0.1831 \text{ m}]}{0.0622 \text{ m}}$$

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	2.2777 W/mK
Φf, flow with ISO10077 panel:	45.5536 W/m
Flow error:	0.000003
Triangles:	5114

Frame width Bf: 62.23 mm Panel width Bp: 366.17 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal	20.000	0.1300	
External	0.000	0.0400	
Adiabatic			
Rsi increased	20.000	0.2000	

Project: Aerztehaus Ried

Detail: Stulp aussen

File: Stulp aussen

Client: -

Date: 16/09/2019

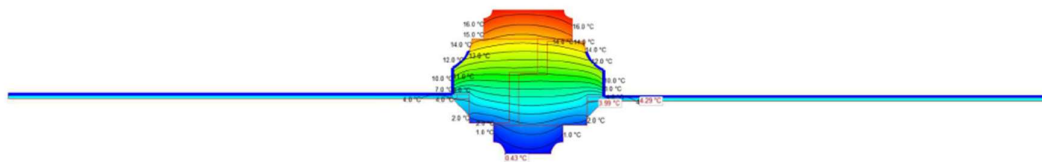
Software: Frame Simulator - 4.0.5 b839 64bit



ψ and condensation comput ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.015 W/mK

Superficial condensation: 472 mm



ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - \sum (U_{x,Bg})}{B_g}$$

$$\psi = \frac{[45.5536 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.6258 \text{ W/m}^2 \text{K} \times 0.0622 \text{ m}]}{0.366 \text{ m}}$$

Glazing transmittance Ug=5.81 W/m²K Frame transmittance Uf=2.63 W/m²K

Glazing size Bg: 366 mm

Frame size Bf: 62 mm

Simulation with glazing

Lp2D, with glazing:	2.2777 W/mK
Φψ, flow with glazing:	45.5536 W/m
Flow error:	0.000003
Triangles:	5114

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Boundary temperatures

Name	L [mm]	Min T. [°C]	Max T. [°C]	Av. T. [°C]	Q [W/m]
Internal	366.17	4.287	16.901	5.799	39.9992
External	460.52	0.431	4.651	3.957	-45.5537
Adiabatic	4.00	4.651	4.884	4.767	0.0000
Rsi increased	120.08	3.991	16.901	10.749	5.5543

Materials

Name	λx [W/mK]	ε	Color
Putty	1.0000	0.900	
Larch	0.1300	0.900	
Glass	1.0000	0.900	
Air	0.0764	0.900	

Project: Aerztehaus Ried

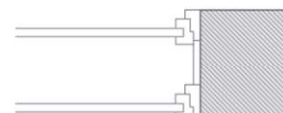
Detail: Stulp aussen

File: Stulp aussen

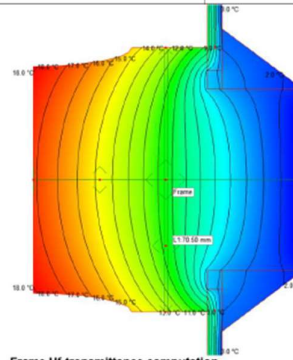
Client: -

Date: 16/09/2019

Software: Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 2.23 W/m²K
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Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Putty	1.0000	0.900	
Larch	0.1300	0.900	

Frame Uf transmittance computation
 $U_f = \frac{1}{\left(\frac{\Phi_f}{\Delta T} \right) - \sum [U_{x,Bp}] / B_f}$
 $U_f = \frac{1}{\left(\frac{46.2199 \text{ W/m}^2}{20.00 \text{ °C}} \right) - \left[\frac{5.7471 \text{ W/m}^2 \cdot \text{K} \cdot 0.1903 \text{ m}}{1} + \frac{5.7471 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}}{1} \right] / 0.0705 \text{ m}}$

Simulation with ISO10077 panel
 Lf2D, with ISO10077 panel: 2.3110 W/mK
 Φf, flow with ISO10077 panel: 46.2199 W/m
 Flow error: 0.000001
 Triangles: 1617

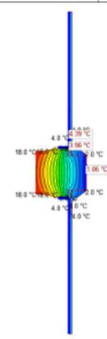
Boundary conditions

Name	Col	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic			
Rsi increased		20.000	0.2000

Project:	Aerztehaus Ried	Detail:	Kaempfer aussen	File:	Kaempfer aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: -0.032 W/mK Superficial condensation: 480 mm
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ψ computation
 $\psi = \frac{\Phi_{\psi}}{\Delta T} - \sum [U_{x,Bg}]$
 $\psi = \frac{46.2199 \text{ W/m}^2}{20.00 \text{ °C}} - \left[\frac{2.2256 \text{ W/m}^2 \cdot \text{K} \cdot 0.0705 \text{ m}}{1} + \frac{5.7471 \text{ W/m}^2 \cdot \text{K} \cdot 0.1903 \text{ m}}{1} + \frac{5.7471 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}}{1} \right]$

Glazing transmittance Ug=5.75 W/m²K
 Frame transmittance Uf=2.23 W/m²K
 Glazing size Bg: 380 mm
 Frame size Bf: 70 mm

Simulation with glazing
 Lf2D, with glazing: 2.3110 W/mK
 Φψ, flow with glazing: 46.2199 W/m
 Flow error: 0.000001
 Triangles: 1617

Boundary conditions

ID	Name	Col	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic				
3	Rsi increased		20.000	0.2000	65.0

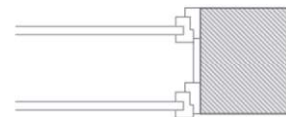
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m²]
Internal	390.50	4.390	18.036	6.926	39.2715
External	470.70	1.064	4.598	3.928	-46.2199
Adiabatic	8.00	4.598	5.057	4.828	-0.0000
Rsi increased	145.60	3.958	18.036	10.458	6.9485

Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Putty	1.0000	0.900	
Larch	0.1300	0.900	

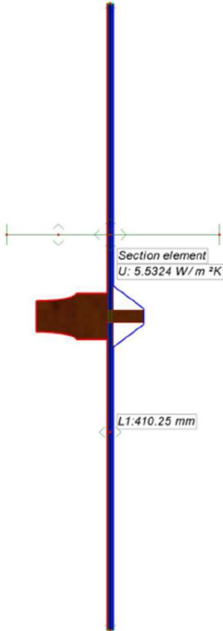
Project:	Aerztehaus Ried	Detail:	Kaempfer aussen	File:	Kaempfer aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Linear thermal bridge computation

EN-ISO 10211:2008

Linear transmittance ψ : -0.0028 W/mK



ψ Computation

$\psi = [\Phi / \Delta T] \cdot \Sigma [UxL]$
 $\psi = [45.3374 \text{ W/m}^2 / 20.00 \text{ }^\circ\text{C}] \cdot [2.2696 \text{ W/mK}]$

L1D Computation (2.2696 W/mK)

$U1 \cdot l1 = [5.5324 \text{ W/m}^2\text{K} \times 0.4102 \text{ m}] = 2.2696 \text{ W/mK}$
 $U2 \cdot l2 = [- \times -] = -$
 $U3 \cdot l3 = [- \times -] = -$
 $U4 \cdot l4 = [- \times -] = -$

Boundary conditions

Name	Col	Air T [°C]	R type	R [m²K/W]
Adiabatic			Constant	-
Internal	20.000		ISO 6946 Internal	-
External	0.000		Constant	0.0400

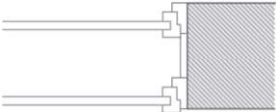
Materials

Name	lx [W/mK]	ε	Color
Glass	1.0000	0.900	
Putty	1.0000	0.900	
Larch	0.1300	0.900	

L2D with bridge	2.2669 W/mK
L1D without bridge	2.2696 W/mK
ΔTemperatures:	20.00 °C
Average flux with bridge	45.3374 W/m²
Flux without bridge	45.3930 W/m²
Flux error	0.000001

Project :	Aerztehaus Ried	Detail:	Sprosse aussen	File:	Sprosse aussen
Reference :	-	Date:	16/09/2019	Software:	Mold Simulator - 4.0.5 b839 64bit

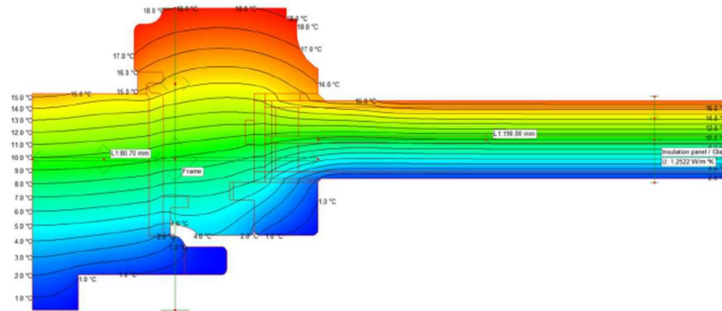
Mold Simulator



Energieeffizienter Prototyp für Kastenfenster

Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.43 W/m²K



Materials

Name	λx [W/mK]	ε	Color
EPDM	0.2500	0.900	
Box 1	0.6100	0.900	
Norway spruce	0.1100	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Cripto	0.9890	0.900	
Cripto	1.0432	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Silicone filled	0.5000	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \left(\frac{\Phi_f}{\Delta T} \right) - \sum \left(U_{x,Bp} \right) / B_f$$

$$U_f = \left(\left(9.9157 \text{ W/m}^2 / 20.00 \text{ °C} \right) - \left(1.7965 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m} \right) / 0.0807 \text{ m} \right)$$

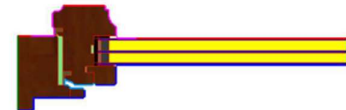
Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	0.4958 W/mK
Φf, flow with ISO10077 panel:	9.9157 W/m
Flow error:	0.000008
Triangles:	11149

Frame width Bf: 80.70 mm Panel width Bp: 190.00 mm

Boundary conditions

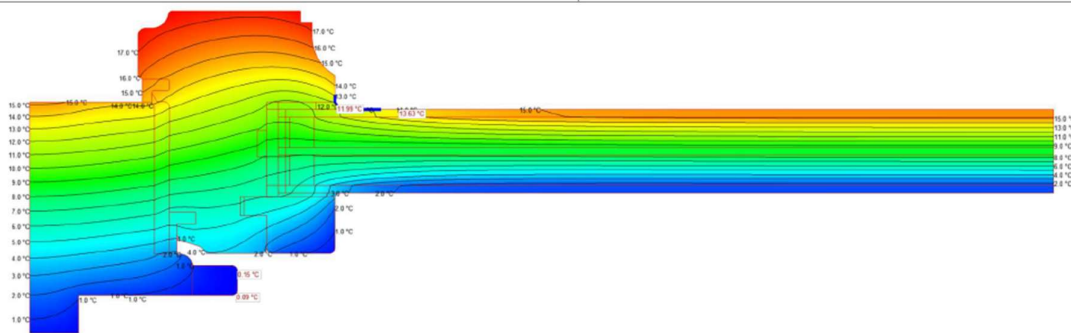
Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000
Rs external cavities		0.000	0.3000



Project:	Aufschnaiter Schule	Detail:	Rahmen o,u,l,r innen	File:	Rahmen o_u_l_r innen	
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit	

ψ and condensation computation
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.039 W/mK
Superficial condensation: 23 mm



ψ computation

$$\psi = \left(\frac{\Phi_{\psi}}{\Delta T} \right) - \sum \left(U_{gxBg} \right)$$

$$\psi = \left(\left(9.9157 \text{ W/m}^2 / 20.00 \text{ °C} \right) - \left(1.4304 \text{ W/m}^2 \text{K} \times 0.0807 \text{ m} \right) - \left(1.7965 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m} \right) / 0.0807 \text{ m} \right)$$

Simulation with glazing

Lf2D, with glazing:	0.4958 W/mK
Φψ, flow with glazing:	9.9157 W/m
Flow error:	0.000008
Triangles:	11149

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0
5	Rs external cavities		0.000	0.3000	65.0

Materials

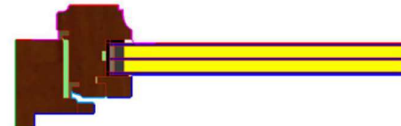
Name	λx [W/mK]	ε	Color
EPDM	0.2500	0.900	
Box 1	0.6100	0.900	
Norway spruce	0.1100	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Cripto	0.9890	0.900	
Cripto	1.0432	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Silicone filled	0.5000	0.900	

Name	λx [W/mK]	ε	Color
10077 radiosity	-	0.900	

Glazing transmittance Ug=1.80 W/m²K Frame transmittance Uf=1.43 W/m²K
Glazing size Bg: 190 mm Frame size Bf: 81 mm

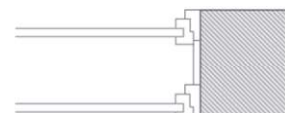
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	218.19	13.627	17.766	15.469	7.6044
External	292.38	0.090	3.526	1.294	-9.4558
Adiabatic	82.99	0.528	15.317	7.346	0.0006
Rsi increased	96.08	11.960	17.766	16.189	2.3114
Rs external cavities	51.44	0.154	4.381	2.682	-0.4598



Project:	Aufschnaiter Schule	Detail:	Rahmen o,u,l,r innen	File:	Rahmen o_u_l_r innen	
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit	

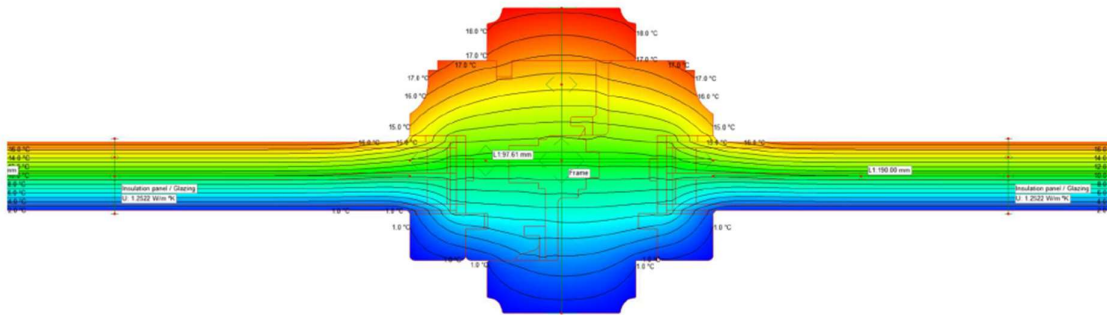
Kastenfenster





Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.37 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
Cripto	1.0473	0.900	
Cripto	0.9885	0.900	
Cripto	1.0470	0.900	
Cripto	0.9885	0.900	
Norway spruce	0.1100	0.900	
Putty	0.5000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Glass	1.0000	0.900	
EPDM	0.2500	0.900	
ISO10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum (U_{x,Bp}) / B_f}{B_f}$$

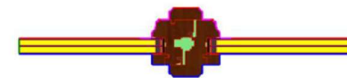
$$U_f = \frac{([17.6212 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.7955 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [1.7956 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}])}{0.0976 \text{ m}}$$

Simulation with ISO10077 panel

Ly2D, with ISO10077 panel:	0.8811 W/mK
Φf, flow with ISO10077 panel:	17.6212 W/m
Flow error:	0.000002
Triangles:	12638

Boundary conditions

Name	Col	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000



Project: Aufschnaiter Schule
Client: -

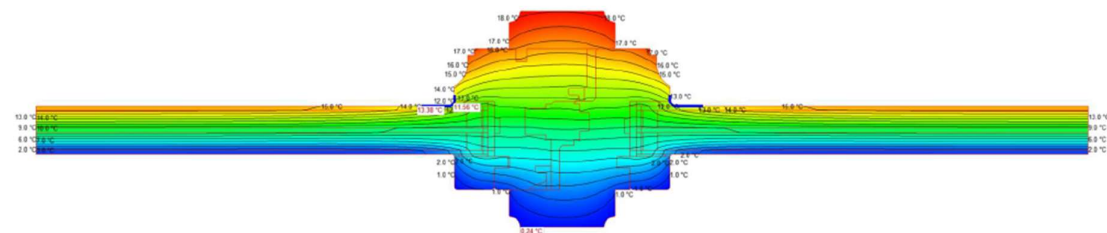
Detail: Stulp innen
Date: 16/09/2019

File: Stulp innen
Software: Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.065 W/mK
Superficial condensation: 45 mm



ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - [U_f \times B_f] - \sum [U_{g,Bg}]}{B_{\psi}}$$

$$\psi = \frac{[17.6212 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.3738 \text{ W/m}^2 \text{K} \times 0.0976 \text{ m}] - [1.7955 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [1.7956 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]}{0.0976 \text{ m}}$$

Glazing transmittance Ug=1.80 W/m²K

Frame transmittance Uf=1.37 W/m²K

Glazing size Bg: 380 mm

Frame size Bf: 98 mm

Simulation with glazing

Ly2D, with glazing:	0.8811 W/mK
Φψ, flow with glazing:	17.6212 W/m
Flow error:	0.000002
Triangles:	12638

Boundary conditions

ID	Name	Col	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

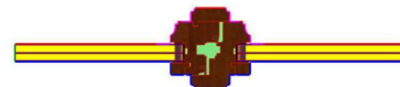
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	391.61	13.381	18.338	15.384	13.9056
External	540.66	0.237	3.269	1.304	-17.6212
Adiabatic	44.00	1.430	15.314	8.448	-0.0000
Rsi increased	158.20	11.557	18.338	15.303	3.7155

Materials

Name	λx [W/mK]	ε	Color
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
Cripto	1.0473	0.900	
Cripto	0.9885	0.900	
Cripto	1.0470	0.900	
Cripto	0.9885	0.900	
Norway spruce	0.1100	0.900	
Putty	0.5000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	

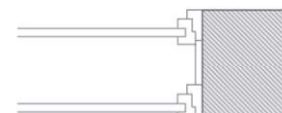
Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
EPDM	0.2500	0.900	
ISO10077 radiosity	-	0.900	



Project: Aufschnaiter Schule
Client: -

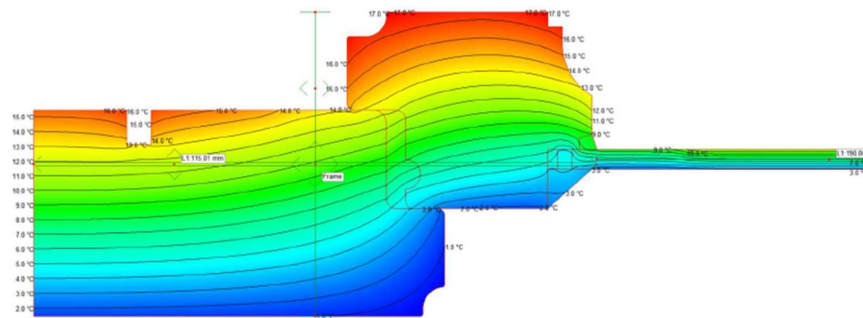
Detail: Stulp innen
Date: 16/09/2019

File: Stulp innen
Software: Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 2.06 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Norway spruce	0.1100	0.900	
Putty	0.5000	0.900	
ISO10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \left(\frac{\Phi_f}{\Delta T} \right) - \Sigma [U_{x,Bp}] / B_f$$

$$U_f = \left(\frac{26.4197 \text{ W/m}^2 / 20.00 \text{ °C}}{5.7472 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}} \right) - \frac{1.1150 \text{ m}}{0.1150 \text{ m}}$$

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	1.3210 W/mK
Φf, flow with ISO10077 panel:	26.4197 W/m
Flow error:	0.000012
Triangles:	8118

Frame width Bf: 115.01 mm Panel width Bp: 190.00 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000
Rs internal cavities		20.000	0.3000



Project:	Aufschnaiter Schule	Detail:	Rahmen oo,ol,or aussen	File:	Rahmen oo_ol_or aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit

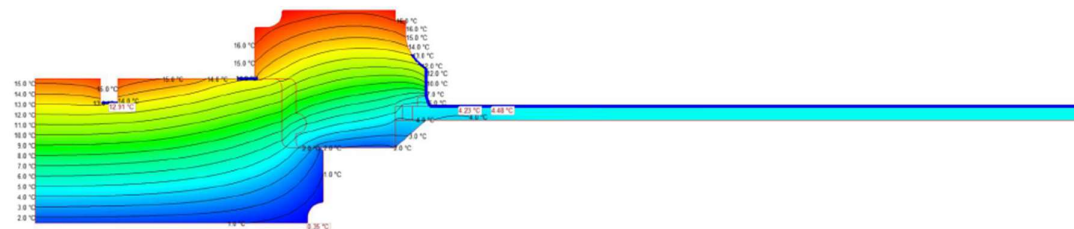


Frame Simulator

ψ and condensation compute
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.008 W/mK

Superficial condensation: 250 mm



ψ computation

$$\psi = \left(\frac{\Phi_{\psi}}{\Delta T} \right) - \Sigma [U_{gxBg}]$$

$$\psi = \left(\frac{26.4197 \text{ W/m}^2 / 20.00 \text{ °C}}{5.7472 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}} \right) - \frac{1.1150 \text{ m}}{0.1150 \text{ m}}$$

Simulation with glazing

Lg2D, with glazing:	1.3210 W/mK
Φψ, flow with glazing:	26.4197 W/m
Flow error:	0.000012
Triangles:	8118

Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Norway spruce	0.1100	0.900	
Putty	0.5000	0.900	
ISO10077 radiosity	-	0.900	

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0
4	Rs internal cavities		20.000	0.3000	65.0

Glazing transmittance Ug=5.75 W/m²K

Frame transmittance Uf=2.06 W/m²K

Glazing size Bg: 190 mm

Frame size Bf: 115 mm

Boundary temperatures

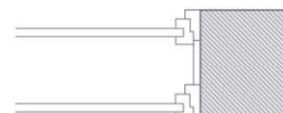
Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	249.01	4.484	16.987	8.345	22.3242
External	329.68	0.349	4.598	3.206	-26.4195
Adiabatic	46.00	1.447	15.407	8.118	0.0004
Rsi increased	94.04	4.234	16.987	12.056	3.7353
Rs internal cavities	19.00	12.912	16.051	14.311	0.3603



Project:	Aufschnaiter Schule	Detail:	Rahmen oo,ol,or aussen	File:	Rahmen oo_ol_or aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit

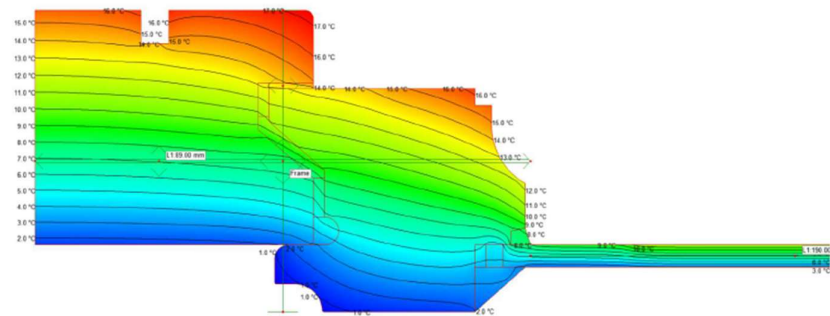


Frame Simulator



Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 2.11 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Norway spruce	0.1100	0.900	
Putty	0.5000	0.900	
ISO10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \left(\frac{\Phi_f}{\Delta T} \right) - \sum \left[\frac{U_{x,Bp}}{B_f} \right]$$

$$U_f = \left(\frac{25.4092 \text{ W/m}^2}{20.00 \text{ °C}} \right) - \left[\frac{5.7471 \text{ W/m}^2 \times 0.1900 \text{ m}}{0.0890 \text{ m}} \right]$$

Simulation with ISO10077 panel

Uf2D, with ISO10077 panel:	1.2705 W/mK
Φf, flow with ISO10077 panel:	25.4092 W/m
Flow error:	0.000005
Triangles:	5097

Frame width Bf: 89.00 mm Panel width Bp: 190.00 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000
Rs internal cavities		20.000	0.3000

Project:	Aufschnaiter Schule	Detail:	Rahmen ul.ur aussen	File:	Rahmen ul_ur aussen
Client:	-	Date:	17/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation
ISO 10077-2 (2017) - radiosity
Linear transmittance ψ: -0.009 W/mK
Superficial condensation: 240 mm



ψ computation

$$\psi = \left(\frac{\Phi_{\psi}}{\Delta T} \right) - \left[\frac{U_f \times B_f}{B_g} \right] - \sum \left[\frac{U_{g,Bg}}{B_g} \right]$$

$$\psi = \left(\frac{25.4092 \text{ W/m}^2}{20.00 \text{ °C}} \right) - \left[\frac{2.1072 \text{ W/m}^2 \times 0.0890 \text{ m}}{0.1900 \text{ m}} \right] - \left[\frac{5.7471 \text{ W/m}^2 \times 0.1900 \text{ m}}{0.1900 \text{ m}} \right]$$

Simulation with glazing

Uf2D, with glazing:	1.2705 W/mK
Φψ, flow with glazing:	25.4092 W/m
Flow error:	0.000005
Triangles:	5097

Materials

Name	λx [W/mK]	ε	Color
Glass	1.0000	0.900	
Norway spruce	0.1100	0.900	
Putty	0.5000	0.900	
ISO10077 radiosity	-	0.900	

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0
4	Rs internal cavities		20.000	0.3000	65.0

Glazing transmittance Ug=5.75 W/m²K

Glazing size Bg: 190 mm

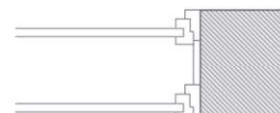
Frame transmittance Uf=2.11 W/m²K

Frame size Bf: 89 mm

Boundary temperatures

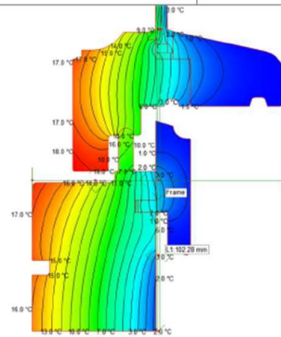
Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	232.00	4.439	17.244	7.852	21.6801
External	294.82	0.495	4.598	3.447	-25.4093
Adiabatic	46.00	1.557	15.653	8.436	-0.0000
Rsi increased	78.69	4.118	17.246	11.233	3.4494
Rs internal cavities	17.00	13.918	16.565	15.064	0.2797

Project:	Aufschnaiter Schule	Detail:	Rahmen ul.ur aussen	File:	Rahmen ul_ur aussen
Client:	-	Date:	17/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance U_f : 2.14 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Norway spruce	0.1100	0.900	
EPDM	0.2500	0.900	
Standard	1.0000	0.900	
Putty	0.5000	0.900	
10077 radiosity	-	0.900	

Frame U_f transmittance computation

$$Uf = ([\Phi f / \Delta T] - \sum [Ux Bp]) / Bf$$

$$Uf = ([25.9550 \text{ W/m} / 20.00 \text{ }^{\circ}\text{C}] - [5.7471 \text{ W/m}^2\text{K} \times 0.1890 \text{ m}] - [-x]) / 0.1023 \text{ m}$$

Simulation with ISO10077 panel	
Lf2D, with ISO10077 panel:	1.2978 W/mK
Φ_f , flow with ISO10077 panel:	25.9550 W/m
Flow error:	0.000012
Triangles:	8007

Boundary conditions

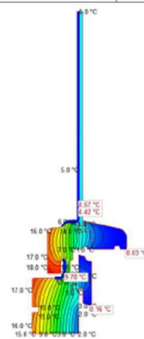
Name	Col.	Air T [°C]	R [m²K/W]
Internal	Red	20.000	0.1300
External	Green	0.000	0.0400
Adiabatic	Blue	-	-
Rs1 increased	Magenta	20.000	0.2000
Rs internal cavities	Orange	20.000	0.3000
Rs external cavities	Light Blue	0.000	0.3000

Project:	Aufschnaiter Schule	Detail:	Rahmen uu aussen	File:	Rahmen uu aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b389 64bit



Frame Simulator

ψ and condensation computation: Linear transmittance ψ : -0.008 W/mK
 ISO 10077-2 (2017) - radiosity
 Superficial condensation: 279 mm



ψ computation

$$\psi = [\Phi \psi / \Delta T] - [Uf \times Bf] - \Sigma [Ug \times Bg]$$

$$\psi = [25.9550 \text{ W/m}^2 / 20.00^\circ\text{C}] - [2.1444 \text{ W/m}^2\text{K}^0.1023 \text{ m}] - [5.7471 \text{ W/m}^2\text{K}^0.1890 \text{ m}] - [-^\circ]$$

Simulation with glazing	
L ψ 2D, with glazing:	1.2978 W/mK
$\Phi\psi$, flow with glazing:	25.9550 W/m
Flow error:	0.000012
Triangles:	8007

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m ² K/W]	H [%]
0	Internal		20 000	0 1300	65.0
1	External		0 000	0 0400	65.0
2	Adiabatic		-	-	65.0
3	RsI increased		20 000	0 2000	65.0
4	Rs internal cavities		20 000	0 3000	65.0
5	Rs external cavities		0 000	0 3000	65.0

Glazing transmittance $U_g=5.75 \text{ W/m}^2\text{K}$ Frame transmittance $U_f=2.14 \text{ W/m}^2\text{K}$
Glazing size $B_g: 189 \text{ mm}$ Frame size $B_f: 102 \text{ mm}$

Boundary temperatures

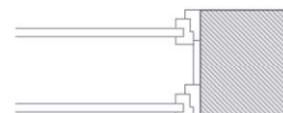
Name	L [mm]	Min T. [°C]	Max T. [°C]	Av. T. [°C]	Q [W/m]
Internal	252.45	4.574	18.378	8.827	21.6959
External	352.95	0.025	4.598	2.767	-24.4200
Adiabatic	46.00	1.722	15.938	8.842	0.0003
Rei increased	66.16	4.416	17.544	11.355	2.8598
Rs internal cavities	74.54	9.698	18.374	14.368	1.3994
Rs external cavities	115.28	0.161	9.951	3.994	-1.5348

Name	λx [W/mK]	ϵ	Color
Norway spruce	0.1100	0.900	
EPDM	0.2500	0.900	
Standard	1.0000	0.900	
Putty	0.5000	0.900	
10077 radiosity	-	0.900	

Project:	Aufschnaiter Schule	Detail:	Rahmen uu aussen	File:	Rahmen uu aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b39 64bit

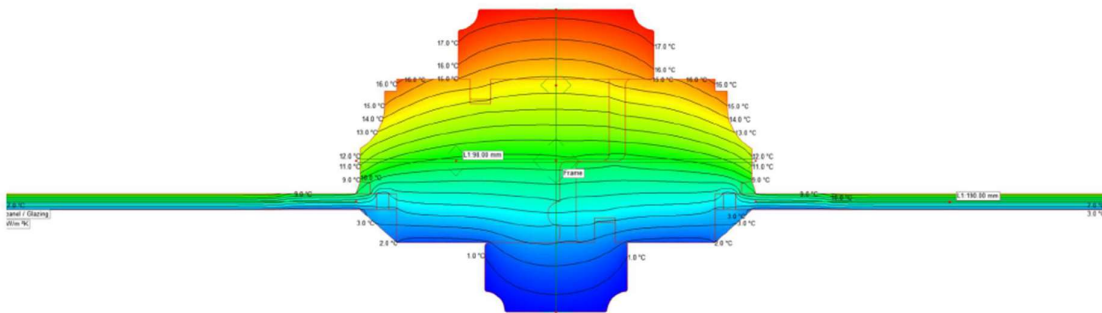


Frame Simulator



Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 2.05 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Putty	0.5000	0.900	
Glass	1.0000	0.900	
Norway spruce	0.1100	0.900	
ISO10077 radiosity	-	0.900	

Frame Uf transmittance computation

$U_f = \frac{1}{\frac{1}{U_{f,gl}} + \frac{1}{U_{f,fr}}}$
 $U_f = \frac{1}{\frac{1}{47.3374 \text{ W/m}^2\text{K}} + \frac{1}{20.00 \text{ °C}} - \frac{5.7471 \text{ W/m}^2\text{K} \times 0.1900 \text{ m}}{0.0980 \text{ m}} - \frac{5.7471 \text{ W/m}^2\text{K} \times 0.1900 \text{ m}}{0.0980 \text{ m}}}$

Simulation with ISO10077 panel

Uf2D, with ISO10077 panel:	2.3669 W/mK
Φf, flow with ISO10077 panel:	47.3374 W/m
Flow error:	0.000001
Triangles:	13046

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rai increased		20.000	0.2000

Project: Aufschnaiter Schule
Client: -

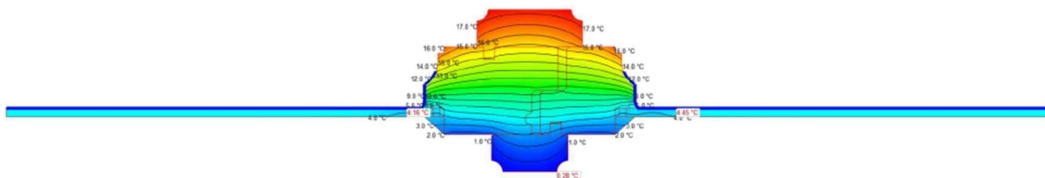
Detail: Stulp aussen
Date: 16/09/2019

File: Stulp aussen
Software: Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.018 W/mK
Superficial condensation: 479 mm



ψ computation

$\psi = \frac{1}{\frac{1}{U_{f,gl}} + \frac{1}{U_{f,fr}}}$
 $\psi = \frac{1}{\frac{1}{47.3374 \text{ W/m}^2\text{K}} + \frac{1}{20.00 \text{ °C}} - \frac{5.7471 \text{ W/m}^2\text{K} \times 0.1900 \text{ m}}{0.0980 \text{ m}} - \frac{5.7471 \text{ W/m}^2\text{K} \times 0.1900 \text{ m}}{0.0980 \text{ m}}}$

Simulation with glazing

Uf2D, with glazing:	2.3669 W/mK
Φψ, flow with glazing:	47.3374 W/m
Flow error:	0.000001
Triangles:	13046

Materials

Name	λx [W/mK]	ε	Color
Putty	0.5000	0.900	
Glass	1.0000	0.900	
Norway spruce	0.1100	0.900	
ISO10077 radiosity	-	0.900	

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rai increased		20.000	0.2000	65.0

Glazing transmittance Ug=5.75 W/m²K

Frame transmittance Uf=2.05 W/m²K

Glazing size Bg: 380 mm

Frame size Bf: 98 mm

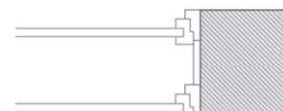
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	388.00	4.454	17.770	6.403	40.5811
External	514.19	0.281	4.598	3.683	-47.3374
Adiabatic	8.00	4.598	5.058	4.828	-0.0000
Rai increased	166.77	4.160	17.770	11.898	6.7563

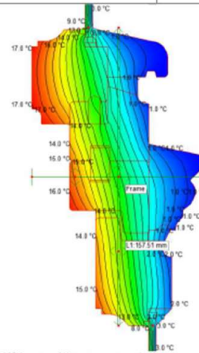
Project: Aufschnaiter Schule
Client: -

Detail: Stulp aussen
Date: 16/09/2019

File: Stulp aussen
Software: Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation
 Simplified ISO 10077-2 (2017) - single eq. cond. **Transmittance Uf: 2.14 W/m²K**



Materials

Name	λx [W/mK]	ε	Color
European larch	0.1300	0.900	
Glass	1.0000	0.900	
Silicone filled	0.5000	0.900	
EPDM	0.2500	0.900	
TPE with mineral additives	0.1800	0.900	
10077 single eq. cond.	-	0.900	
10077 single eq. cond. slightly vent.	-	0.900	
10077 single eq. cond.	-	0.900	

Frame Uf transmittance computation

$$U_f = ([\Phi_f / \Delta T] - \sum [U_{x,Bp}] / B) / B$$

$$U_f = ([50.2097 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.7471 \text{ W/m}^2 \times 0.1900 \text{ m}] - [5.7472 \text{ W/m}^2 \times 0.1910 \text{ m}]) / 0.1575 \text{ m}$$

Simulation with ISO10077 panel:

LF2D, with ISO10077 panel:	2.5105 W/mK
Φf, flow with ISO10077 panel:	50.2097 W/m
Flow error:	0.000000
Triangles:	14588

Frame width Bf: 157.51 mm Panel width Bp: 380.97 mm

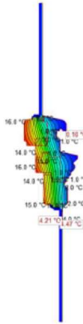
Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rai increased		20.000	0.2000

Project:	Aufschnaiter Schule	Detail:	Kaempfer aussen	File:	Kaempfer aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation
 Simplified ISO 10077-2 (2017) - single eq. cond. **Linear transmittance ψ: -0.017 W/mK**
Superficial condensation: 479 mm



ψ computation

$$\psi = [\Phi_{\psi} / \Delta T] - [U_f \times B_f] - \sum [U_{g,Bg}]$$

$$\psi = [50.2097 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.1433 \text{ W/m}^2 \times 0.1575 \text{ m}] - [5.7471 \text{ W/m}^2 \times 0.1900 \text{ m}] - [5.7472 \text{ W/m}^2 \times 0.1910 \text{ m}]$$

Glazing transmittance Ug=5.75 W/m²K Frame transmittance Uf=2.14 W/m²K

Glazing size Bg: 381 mm

Frame size Bf: 158 mm

Simulation with glazing

LF2D, with glazing:	2.5105 W/mK
Φψ, flow with glazing:	50.2097 W/m
Flow error:	0.000000
Triangles:	14588

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rai increased		20.000	0.2000	65.0

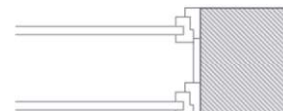
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	446.89	4.472	16.966	7.447	43.1512
External	632.89	0.096	4.879	3.173	-50.2097
Adiabatic	8.00	4.598	5.067	4.828	-0.0000
Rai increased	170.19	4.209	16.966	11.705	7.0565

Materials

Name	λx [W/mK]	ε	Color
European larch	0.1300	0.900	
Glass	1.0000	0.900	
Silicone filled	0.5000	0.900	
EPDM	0.2500	0.900	
TPE with mineral additives	0.1800	0.900	
10077 single eq. cond.	-	0.900	
10077 single eq. cond. slightly vent.	-	0.900	
10077 single eq. cond.	-	0.900	

Project:	Aufschnaiter Schule	Detail:	Kaempfer aussen	File:	Kaempfer aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit

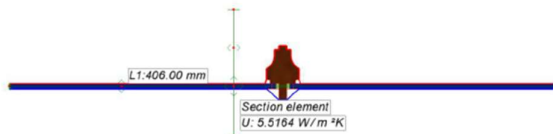


Linear thermal bridge computation	-
EN-ISO 10211:2008	-
Linear transmittance ψ : 0.0067 W/mK	-

ψ Computation	
$\psi = [\Phi / \Delta T] - \sum [UxL]$	L2D with bridge 2.2464 W/mK
$\psi = [44.9279 \text{ W/m}^2 / 20.00 \text{ }^\circ\text{C}] - [2.2397 \text{ W/mK}]$	L1D without bridge 2.2397 W/mK
L1D Computation (2.2397 W/mK)	Δ Temperatures: 20.00 °C
$U1*11 = [5.5164 \text{ W/m}^2\text{K} \times 0.4060 \text{ m}] = 2.2397 \text{ W/mK}$	Average flux with bridge 44.9279 W/m
$U2*12 = [-x] = -$	Flux without bridge 44.7932 W/m
$U3*13 = [-x] = -$	Flux error 0.000001
$U4*14 = [-x] = -$	

Name	Col	Air T [°C]	R type	R [m²K/W]
Adiabatic			Constant	-
Internal	20.000		ISO 6946 Internal	-
External	0.000		Constant	0.0400

Name	λ [W/mK]	ϵ	Color
Glass	1.0000	0.900	
Putty	1.0000	0.900	
Norway spruce	0.1100	0.900	
10077 radiosity	-	0.900	



Project :	Aufschnaiter Schule	Detail:	Sprosse aussen	File:	Sprossen aussen
Reference :	-	Date:	16/09/2019	Software:	Mold Simulator - 4.0.5 b839 64bit

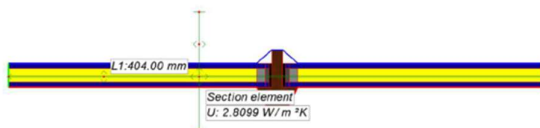


Linear thermal bridge computation	-
EN-ISO 10211:2008	-
Linear transmittance ψ : 0.0830 W/mK	-

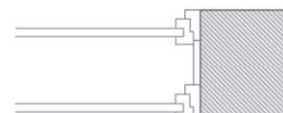
ψ Computation	
$\psi = [\Phi / \Delta T] - \sum [UxL]$	L2D with bridge 1.2182 W/mK
$\psi = [24.3643 \text{ W/m}^2 / 20.00 \text{ }^\circ\text{C}] - [1.1352 \text{ W/mK}]$	L1D without bridge 1.1352 W/mK
L1D Computation (1.1352 W/mK)	Δ Temperatures: 20.00 °C
$U1*11 = [2.8099 \text{ W/m}^2\text{K} \times 0.4040 \text{ m}] = 1.1352 \text{ W/mK}$	Average flux with bridge 24.3643 W/m
$U2*12 = [-x] = -$	Flux without bridge 22.7039 W/m
$U3*13 = [-x] = -$	Flux error 0.000002
$U4*14 = [-x] = -$	

Name	Col	Air T [°C]	R type	R [m²K/W]
Adiabatic			Constant	-
Internal	20.000		ISO 6946 Internal	-
External	0.000		Constant	0.0400

Name	λ [W/mK]	ϵ	Color
Argon	1.0217	0.900	
Argon	1.0216	0.900	
Larch	0.1300	0.900	
Butyl (isobutylene) solid/hot melt	0.2400	0.900	
Glass	1.0000	0.900	
Putty	0.5000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	

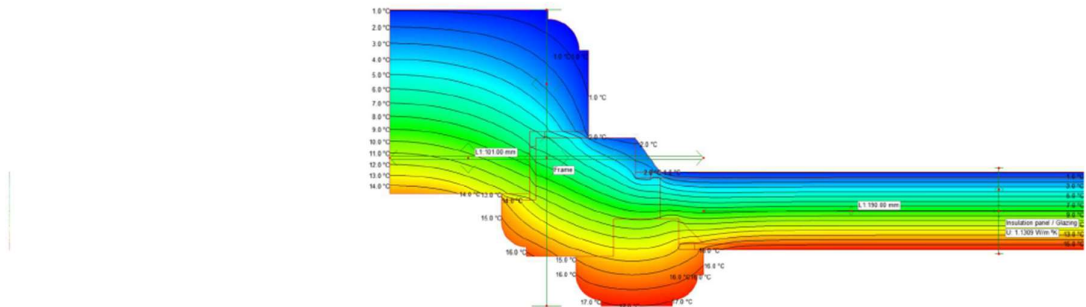


Project :	Dante Schule	Detail:	Sprosse innen	File:	Sprosse innen
Reference :	-	Date:	16/09/2019	Software:	Mold Simulator - 4.0.5 b839 64bit



Werte für typische Verbundfenster 1910er/1920er Jahre

Frame Uf computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 1.90 W/m²K
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Name	λx [W/mK]	ε	Color
European larch	0.1300	0.900	
Glass	1.0000	0.900	
EPDM	0.2500	0.900	
Silicone	0.5000	0.900	
Air	1.2302	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum (U_{x,Bp}) / B_f}{B_f}$$

$$U_f = \frac{[(14.8524 \text{ W/m}^2 / 20.00 \text{ °C}) - (2.8081 \text{ W/m}^2 \cdot \text{K} \times 0.1900 \text{ m}) / 0.1010 \text{ m}]}{0.1010 \text{ m}}$$

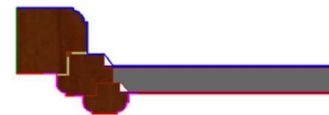
Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	0.7426 W/mK
Φf, flow with ISO10077 panel:	14.8524 W/m
Flow error:	0.000001
Triangles:	6984

Frame width Bf: 101.00 mm Panel width Bp: 190.00 mm

Boundary conditions

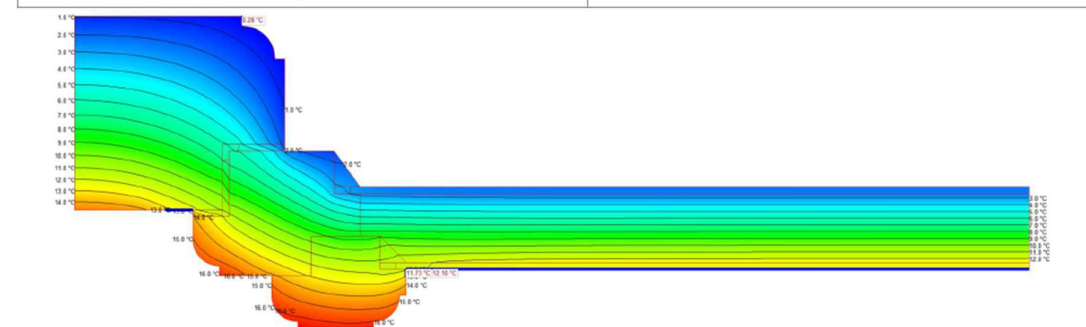
Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000



Project:	Dante Schule	Detail:	Rahmen L_r_o	File:	Rahmen L_r_o
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: 0.017 W/mK Superficial condensation: 215 mm
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ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - [U_f \times B_f] - \sum [U_{g,Bg}]}{B_{\psi}}$$

$$\psi = \frac{[(14.8524 \text{ W/m}^2 / 20.00 \text{ °C}) - (1.8975 \text{ W/m}^2 \cdot \text{K} \times 0.1010 \text{ m}) - (2.8081 \text{ W/m}^2 \cdot \text{K} \times 0.1900 \text{ m})] / 0.1010 \text{ m}}{0.1010 \text{ m}}$$

Simulation with glazing

Lp2D, with glazing:	0.7426 W/mK
Φψ, flow with glazing:	14.8524 W/m
Flow error:	0.000001
Triangles:	6984

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Glazing transmittance Ug=2.81 W/m²K

Glazing size Bg: 190 mm

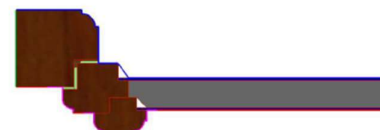
Frame transmittance Uf=1.90 W/m²K

Frame size Bf: 101 mm

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	237.00	12.097	16.860	13.299	12.2162
External	333.31	0.285	2.752	1.762	-14.8524
Adiabatic	84.00	0.958	14.771	7.290	0.0007
Rsi increased	97.70	11.734	16.860	14.603	2.6363

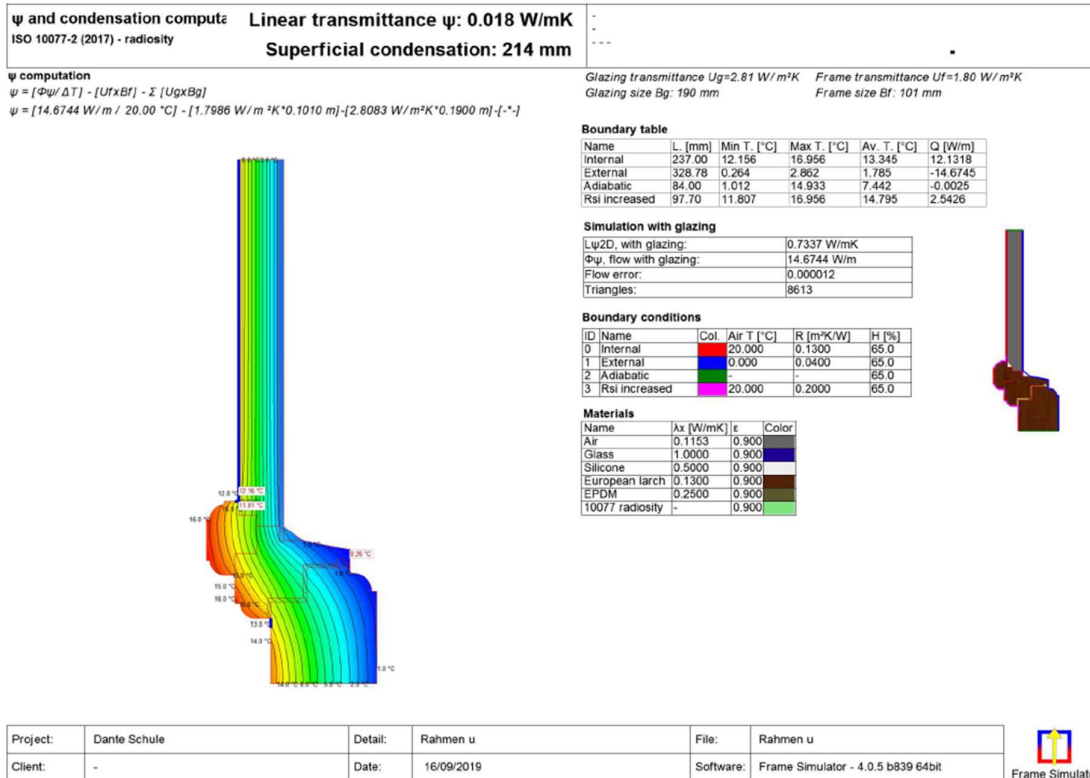
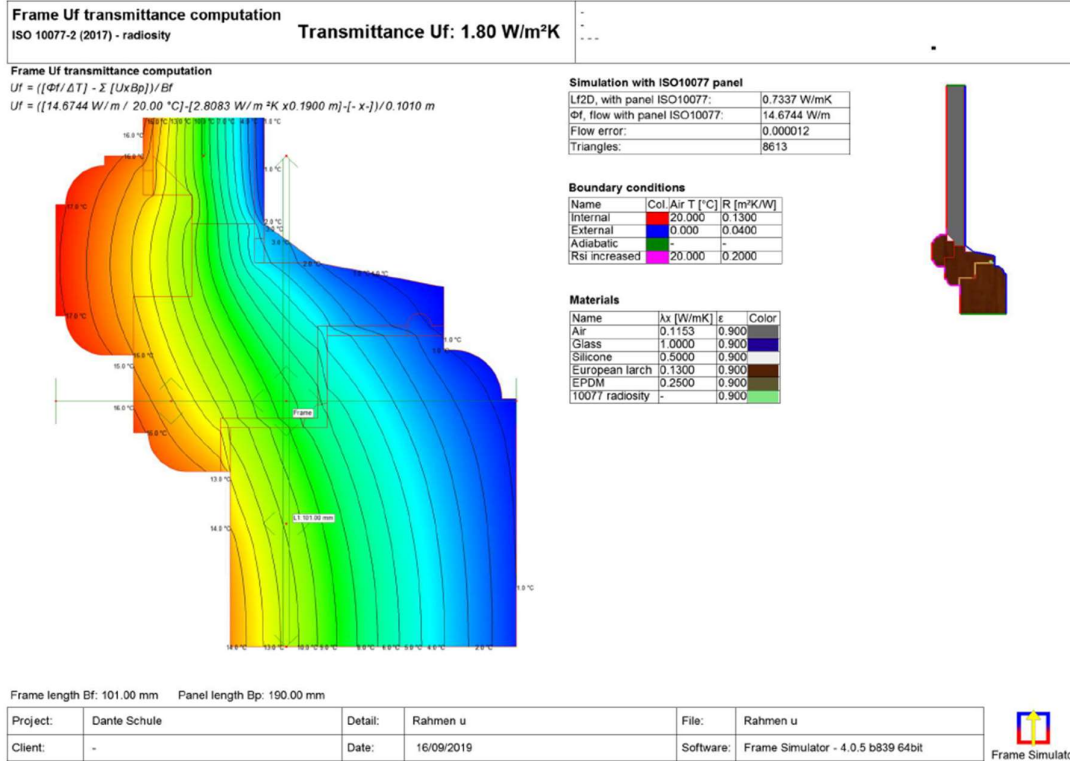
Name	λx [W/mK]	ε	Color
European larch	0.1300	0.900	
Glass	1.0000	0.900	
EPDM	0.2500	0.900	
Silicone	0.5000	0.900	
Air	1.2302	0.900	
10077 radiosity	-	0.900	



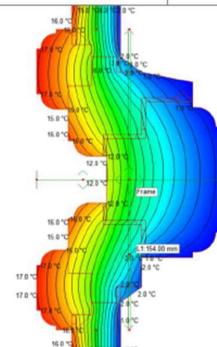
Project:	Dante Schule	Detail:	Rahmen L_r_o	File:	Rahmen L_r_o
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Verbundfenster 1910er/1920er Jahre



Frame Uf computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 1.87 W/m²K
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Materials

Name	λx [W/mK]	ε	Color
PVC Dichtung	0.1400	0.900	
Air	0.1153	0.900	
Glass	1.0000	0.900	
Air	0.1153	0.900	
Silicone filled	0.5000	0.900	
European larch	0.1300	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \left(\frac{\Phi_f}{\Delta T} \right) - \sum \left(U_{x,Bp} \right) / B_f$$

$$U_f = \left(\frac{27.8219 \text{ W/m}^2 / 20.00 \text{ °C}}{0.1540 \text{ m}} \right) - \left(\frac{2.8081 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}}{0.1540 \text{ m}} \right) - \left(\frac{2.8082 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}}{0.1540 \text{ m}} \right)$$

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	1.3911 W/mK
Φf, flow with ISO10077 panel:	27.8219 W/m
Flow error:	0.000001
Triangles:	14014

Frame width Bf: 154.00 mm Panel width Bp: 380.00 mm

Boundary conditions

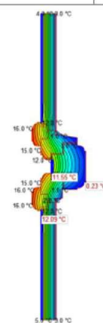
Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000



Project:	Dante Schule	Detail:	Kaempfer	File:	Kaempfer
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: 0.035 W/mK Superficial condensation: 440 mm
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ψ computation

$$\psi = \left(\frac{\Phi_{\psi}}{\Delta T} \right) - \sum \left(U_{g,Bg} \right)$$

$$\psi = \left(\frac{27.8219 \text{ W/m}^2 / 20.00 \text{ °C}}{0.1540 \text{ m}} \right) - \left(\frac{2.8081 \text{ W/m}^2 \text{K} \times 0.1540 \text{ m}}{0.1540 \text{ m}} \right) - \left(\frac{2.8082 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}}{0.1540 \text{ m}} \right)$$

Glazing transmittance Ug=2.81 W/m²K Frame transmittance Uf=1.87 W/m²K

Glazing size Bg: 380 mm

Frame size Bf: 154 mm

Simulation with glazing

Lf2D, with glazing:	1.3911 W/mK
Φψ, flow with glazing:	27.8219 W/m
Flow error:	0.000001
Triangles:	14014

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Avg. T [°C]	Q [W/m]
Internal	426.00	12.086	16.913	13.168	22.3891
External	614.09	0.229	2.819	1.812	-27.8219
Adiabatic	50.00	2.245	12.697	7.471	0.0000
Rsi increased	195.39	11.554	16.913	14.439	5.4328

Materials

Name	λx [W/mK]	ε	Color
PVC Dichtung	0.1400	0.900	
Air	0.1153	0.900	
Glass	1.0000	0.900	
Air	0.1153	0.900	
Silicone filled	0.5000	0.900	
European larch	0.1300	0.900	
10077 radiosity	-	0.900	

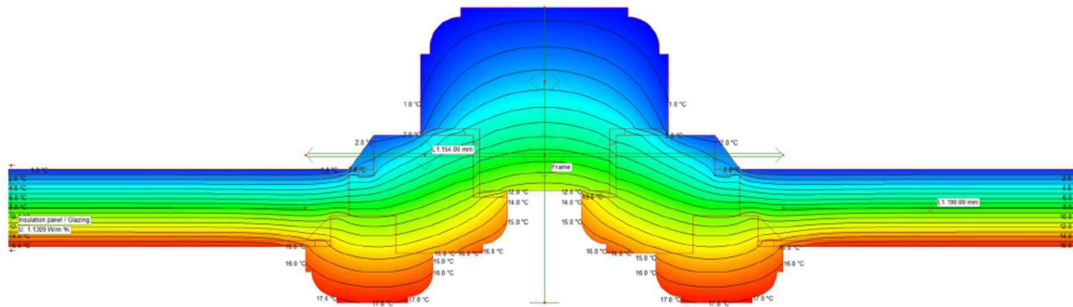


Project:	Dante Schule	Detail:	Kaempfer	File:	Kaempfer
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.93 W/m²K



Materials

Name	Ax [W/mK]	ε	Color
European larch	0.1300	0.900	
Air	1.2302	0.900	
EPDM	0.2500	0.900	
Glass	1.0000	0.900	
Silicone	0.5000	0.900	
Air	1.2302	0.900	
ISO10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum [U_{x,Bp}] / B_f}{\Delta T}$$

$$U_f = \frac{([27.9787 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.8081 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [2.8081 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]) / 0.1540 \text{ m}}$$

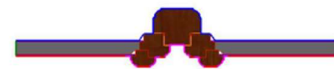
Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	1.3989 W/mK
Φf, flow with ISO10077 panel:	27.9787 W/m
Flow error:	0.000002
Triangles:	13792

Frame width Bf: 154.00 mm Panel width Bp: 380.00 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal	20.000	0.1300	
External	0.000	0.0400	
Adiabatic			
Rsi increased	20.000	0.2000	



Project:	Dante Schule	Detail:	Setzholz	File:	Setzholz
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit

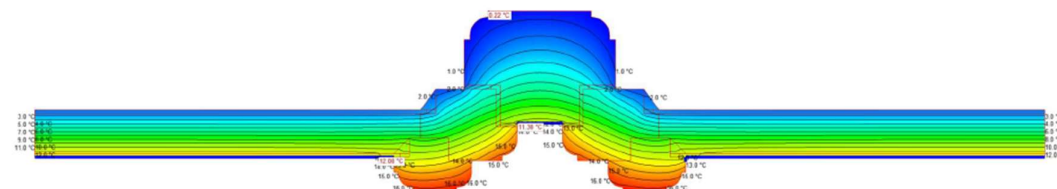


Frame Simulator

ψ and condensation computation
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.034 W/mK

Superficial condensation: 446 mm



ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - \sum [U_{x,Bp}] / B_{\psi}}{\Delta T}$$

$$\psi = \frac{([27.9787 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.9314 \text{ W/m}^2 \text{K} \times 0.1540 \text{ m}] - [2.8081 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [2.8081 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]) / 0.1540 \text{ m}}$$

Glazing transmittance Ug=2.81 W/m²K Frame transmittance Uf=1.93 W/m²K

Glazing size Bg: 380 mm

Frame size Bf: 154 mm

Simulation with glazing

Lp2D, with glazing:	1.3989 W/mK
Φψ, flow with glazing:	27.9787 W/m
Flow error:	0.000002
Triangles:	13792

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal	20.000	0.1300	65.0	
1	External	0.000	0.0400	65.0	
2	Adiabatic				
3	Rsi increased	20.000	0.2000	65.0	

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	426.00	12.083	16.825	13.153	22.4376
External	618.62	0.218	2.628	1.809	-27.9787
Adiabatic	50.00	2.245	12.697	7.470	-0.0000
Rsi increased	195.39	11.380	16.825	14.328	5.5411

Materials

Name	Ax [W/mK]	ε	Color
European larch	0.1300	0.900	
Air	1.2302	0.900	
EPDM	0.2500	0.900	
Glass	1.0000	0.900	
Silicone	0.5000	0.900	
Air	1.2302	0.900	
ISO10077 radiosity	-	0.900	



Project:	Dante Schule	Detail:	Setzholz	File:	Setzholz
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Simulator

Linear thermal bridge computation

EN-ISO 10211:2008

Linear transmittance ψ : 0.0065 W/mK

ψ Computation

$\psi = [\Phi / \Delta T] - \Sigma [UxL]$

$\psi = [44.4089 \text{ W/m}^2 / 20.00 \text{ }^\circ\text{C}] - [2.2139 \text{ W/mK}]$

L2D with bridge 2.2204 W/mK
L1D without bridge 2.2139 W/mK
 ΔT temperatures: 20.00 $^\circ\text{C}$
Average flux with bridge 44.4089 W/m
Flux without bridge 44.2785 W/m
Flux error 0.000000

L1D Computation (2.2139 W/mK)

$U1*11 = [5.5626 \text{ W/m}^2\text{K} \times 0.3980 \text{ m}] = 2.2139 \text{ W/mK}$
 $U2*12 = [-x] = -$
 $U3*13 = [-x] = -$
 $U4*14 = [-x] = -$

Boundary conditions

Name	Col	Air T [°C]	R type	R [m²K/W]
Adiabatic		-	Constant	-
Internal		20.000	ISO 6946 Internal	-
External		0.000	Constant	0.0400

Materials

Name	λ_x [W/mK]	ϵ	Color
European larch	0.1300	0.900	
Putty	0.5000	0.900	
Putty	1.0000	0.900	

Project :	Dante Schule	Detail:	Sprosse aussen	File:	2 - PSI+ISO13788 - 2 environments
Reference :	-	Date:	16/09/2019	Software:	Mold Simulator - 4.0.5 b839 64bit

Linear thermal bridge computation

EN-ISO 10211:2008

Linear transmittance ψ : 0.0075 W/mK

ψ Computation

$\psi = [\Phi / \Delta T] - \Sigma [UxL]$

$\psi = [44.4680 \text{ W/m}^2 / 20.00 \text{ }^\circ\text{C}] - [2.2159 \text{ W/mK}]$

L2D with bridge 2.2234 W/mK
L1D without bridge 2.2159 W/mK
 ΔT temperatures: 20.00 $^\circ\text{C}$
Average flux with bridge 44.4680 W/m
Flux without bridge 44.3184 W/m
Flux error 0.000001

L1D Computation (2.2159 W/mK)

$U1*11 = [5.5676 \text{ W/m}^2\text{K} \times 0.3980 \text{ m}] = 2.2159 \text{ W/mK}$
 $U2*12 = [-x] = -$
 $U3*13 = [-x] = -$
 $U4*14 = [-x] = -$

Boundary conditions

Name	Col	Air T [°C]	R type	R [m²K/W]
Adiabatic		-	Constant	-
Internal		20.000	ISO 6946 Internal	-
External		0.000	Constant	0.0400

Materials

Name	λ_x [W/mK]	ϵ	Color
Glass	1.0000	0.900	
Putty	0.5000	0.900	
European larch	0.1300	0.900	

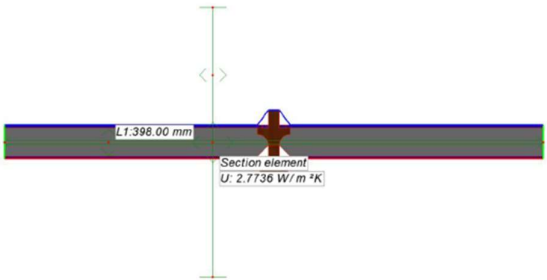
Project :	Dante Schule	Detail:	Sprosse innen	File:	2 - PSI+ISO13788 - 2 environments
Reference :	-	Date:	16/09/2019	Software:	Mold Simulator - 4.0.5 b839 64bit

Linear thermal bridge computation	-
EN-ISO 10211:2008	-
Linear transmittance ψ : 0.0107 W/mK	- - -

ψ Computation $\psi = [\Phi / \Delta T] - \Sigma [UxL]$ $\psi = [22.2919 \text{ W/m} / 20.00 \text{ }^\circ\text{C}] - [1.1039 \text{ W/mK}]$ L1D Computation (1.1039 W/mK) $U1*11 = [2.7736 \text{ W/m}^2\text{K} \times 0.3980 \text{ m}] = 1.1039 \text{ W/mK}$ $U2*12 = [-x] = -$ $U3*13 = [-x] = -$ $U4*14 = [-x] = -$	<table><tr><td>L2D with bridge</td><td>1.1146 W/mK</td></tr><tr><td>L1D without bridge</td><td>1.1039 W/mK</td></tr><tr><td>ΔTemperatures:</td><td>20.00 $^\circ\text{C}$</td></tr><tr><td>Average flux with bridge</td><td>22.2919 W/m</td></tr><tr><td>Flux without bridge</td><td>22.0775 W/m</td></tr><tr><td>Flux error</td><td>0.000002</td></tr></table>	L2D with bridge	1.1146 W/mK	L1D without bridge	1.1039 W/mK	Δ Temperatures:	20.00 $^\circ\text{C}$	Average flux with bridge	22.2919 W/m	Flux without bridge	22.0775 W/m	Flux error	0.000002
L2D with bridge	1.1146 W/mK												
L1D without bridge	1.1039 W/mK												
Δ Temperatures:	20.00 $^\circ\text{C}$												
Average flux with bridge	22.2919 W/m												
Flux without bridge	22.0775 W/m												
Flux error	0.000002												

Boundary conditions			
Name	Col	Air T [$^\circ\text{C}$]	R type
Adiabatic			Constant
Internal	20.000	ISO 8946 Internal	-
External	0.000	Constant	0.0400

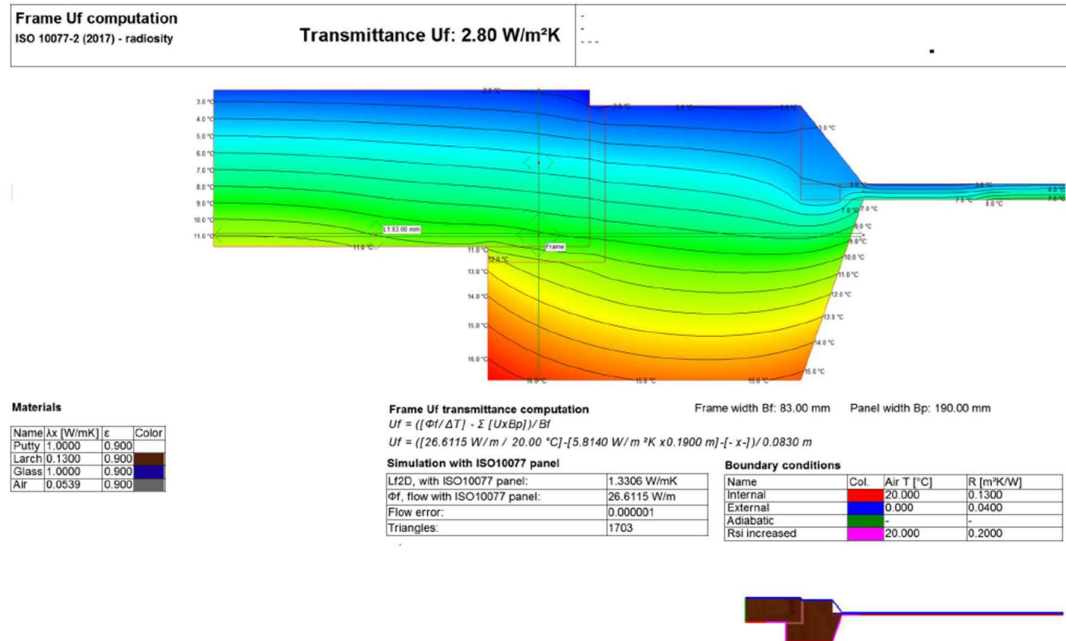
Materials			
Name	lx	W/mK	Color
Glass	1.0000	0.900	
Air	1.1716	0.900	
Putty	0.5000	0.900	
Air	1.1716	0.900	
European larch	0.1300	0.900	



Project :	Dante Schule	Detail:	Sprossen	File:	Sprosse
Reference :	-	Date:	16/09/2019	Software:	Mold Simulator - 4.0.5 b839 64bit

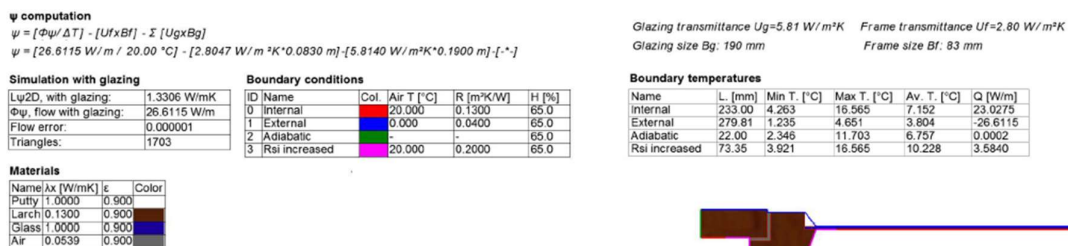


Werte für typische Kastenfenster saniert mit Isolierverglasung (innere Fensterebene)

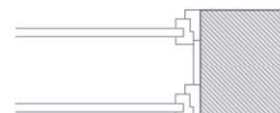


Project:	Knabihof	Detail:	Rahmen o./r aussen	File:	Rahmen o./r aussen	
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit	Frame Simulator

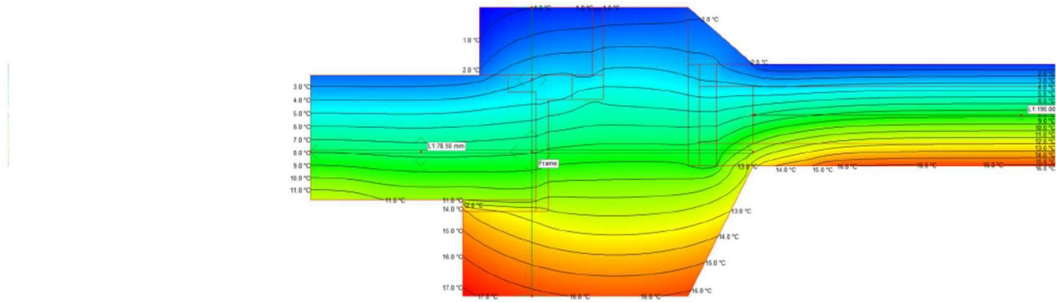
ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: -0.007 W/mK Superficial condensation: 270 mm
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Project:	Knabihof	Detail:	Rahmen o./r aussen	File:	Rahmen o./r aussen	
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit	Frame Simulator



Frame Uf computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 2.40 W/m²K
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Materials

Name	λx [W/mK]	ε	Color
Larch	0.1300	0.900	
EPDM	0.2500	0.900	
Argon	1.0433	0.900	
Glass	1.0000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Putty	0.5000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation
 $U_f = \frac{1}{\frac{1}{\Phi_f / \Delta T} + \sum \frac{1}{U_{x,Bp}}}$
 $U_f = \frac{1}{\frac{1}{15.1075 \text{ W/m}^2 \cdot \text{K}} + \frac{1}{2.8455 \text{ W/m}^2 \cdot \text{K}} + \frac{1}{0.1900 \text{ m}} + \frac{1}{0.0785 \text{ m}}}$

Simulation with ISO10077 panel

L2D, with ISO10077 panel:	0.7554 W/mK
Φf, flow with ISO10077 panel:	15.1075 W/m
Flow error:	0.000008
Triangles:	2218

Boundary conditions

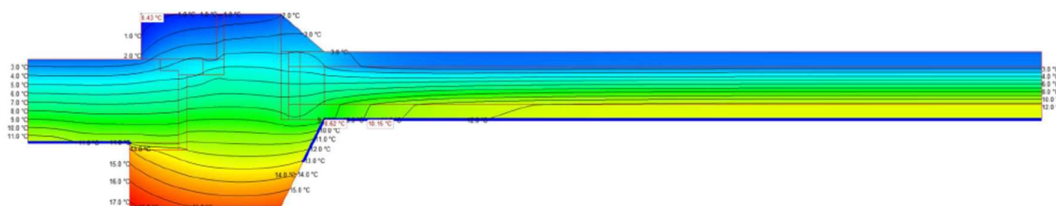
Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000



Project:	Dante Schule	Detail:	Rahmen o.u./r innen	File:	Rahmen o.u./r innen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: 0.026 W/mK Superficial condensation: 247 mm
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ψ computation

$$\psi = \frac{1}{\frac{1}{\Phi_{\psi} / \Delta T} + \sum \frac{1}{U_{x,Bg}}}$$

$$\psi = \frac{1}{\frac{1}{15.1075 \text{ W/m}^2 \cdot \text{K}} + \frac{1}{2.8455 \text{ W/m}^2 \cdot \text{K}} + \frac{1}{0.1900 \text{ m}} + \frac{1}{0.0785 \text{ m}}}$$

Simulation with glazing

L2D, with glazing:	0.7554 W/mK
Φψ, flow with glazing:	15.1075 W/m
Flow error:	0.000008
Triangles:	2218

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Materials

Name	λx [W/mK]	ε	Color
Larch	0.1300	0.900	
EPDM	0.2500	0.900	
Argon	1.0433	0.900	
Glass	1.0000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Putty	0.5000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
10077 radiosity	-	0.900	

Glazing transmittance Ug=2.85 W/m²K

Glazing size Bg: 190 mm

Frame transmittance Uf=2.40 W/m²K

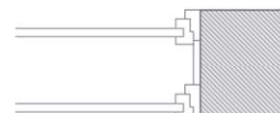
Frame size Bf: 79 mm

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Avg T [°C]	Q [W/m]
Internal	228.50	10.147	17.222	12.928	12.4298
External	284.24	0.431	3.617	2.126	-15.1074
Adiabatic	40.00	2.184	12.595	7.143	-0.0007
Rsi increased	71.21	8.625	17.222	12.480	2.6777

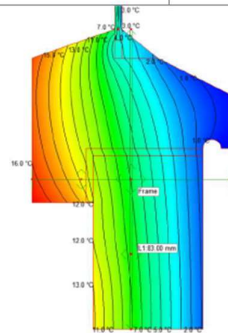


Project:	Dante Schule	Detail:	Rahmen o.u./r innen	File:	Rahmen o.u./r innen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation ISO 10077-2 (2017) - radiosity

Transmittance Uf: 2.41 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Air	0.0827	0.900	
Larch	0.1300	0.900	
Putty	0.5000	0.900	
Glass	1.0000	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum (U_{x,Bp}) / B_f}{B_f}$$

$$U_f = \frac{([25.9661 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.8140 \text{ W/m}^2 \times 0.1900 \text{ m}] - x)}{0.0830 \text{ m}}$$

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	1.2963 W/mK
Φf, flow with ISO10077 panel:	25.9661 W/m
Flow error:	0.000003
Triangles:	2076

Frame width Bf: 83.00 mm Panel width Bp: 190.00 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000

Project:	Dante Schule	Detail:	Rahmen u aussen	File:	Rahmen u aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Simulator

ψ and condensation computation ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: -0.006 W/mK

Superficial condensation: 264 mm



ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - [U_f \times B_f]}{\sum [U_{g,Bg}]}$$

$$\psi = \frac{([25.9661 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.4073 \text{ W/m}^2 \times 0.0830 \text{ m}] - [5.8140 \text{ W/m}^2 \times 0.1900 \text{ m}])}{-}$$

Simulation with glazing

Lp2D, with glazing:	1.2963 W/mK
Φψ, flow with glazing:	25.9661 W/m
Flow error:	0.000003
Triangles:	2076

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

Materials

Name	λx [W/mK]	ε	Color
Air	0.0827	0.900	
Larch	0.1300	0.900	
Putty	0.5000	0.900	
Glass	1.0000	0.900	

Glazing transmittance Ug=5.81 W/m²K Frame transmittance Uf=2.41 W/m²K

Glazing size Bg: 190 mm

Frame size Bf: 83 mm

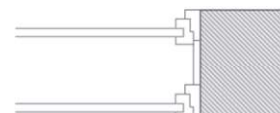
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	233.00	4.339	16.977	7.355	22.6629
External	300.52	0.193	4.651	3.459	-25.9660
Adiabatic	32.50	1.842	13.199	7.233	0.0003
Rsi increased	73.35	4.118	16.977	10.994	3.3032

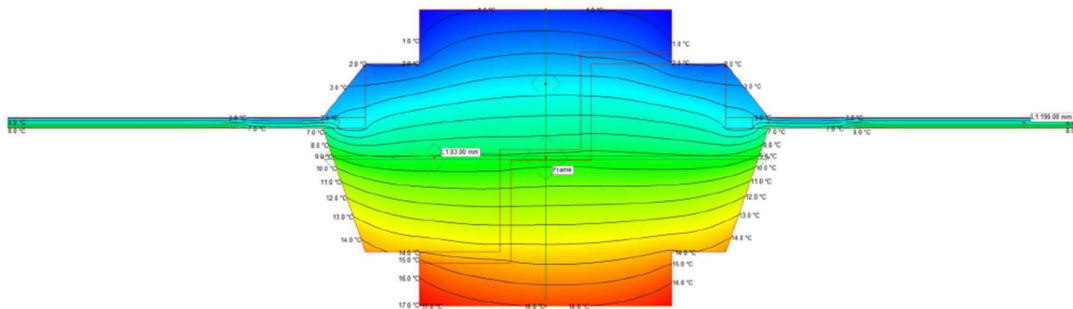
Project:	Dante Schule	Detail:	Rahmen u aussen	File:	Rahmen u aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Simulator



Frame Uf computation ISO 10077-2 (2017) - radiosity - unventilated	Transmittance Uf: 2.34 W/m²K	- - -
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Materials

Name\λx [W/mK]	ε	Color
Glass 1.0000	0.900	
Putty 0.5000	0.900	
Larch 0.1300	0.900	
Air 0.0837	0.900	

Frame Uf transmittance computation

$$U_f = \frac{(\Phi_f / \Delta T) - \sum [U_{x,Bp}] / B_f}{B_f}$$

$$U_f = \frac{[47.8001 \text{ W/m}^2 / 20.00 \text{ °C}] - [5.8140 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [5.8140 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]}{0.0830 \text{ m}}$$

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	2.3900 W/mK
Φf, flow with ISO10077 panel:	47.8001 W/m
Flow error:	0.000001
Triangles:	2080

Frame width Bf: 83.00 mm Panel width Bp: 380.00 mm

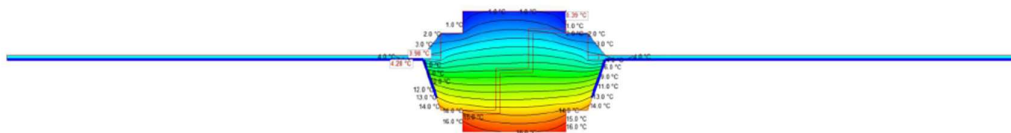
Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rai increased		20.000	0.2000

Project:	Dante Schule	Detail:	Stulp aussen	File:	Stulp aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity - unventilated	Linear transmittance ψ: -0.013 W/mK Superficial condensation: 454 mm	- - -
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ψ computation

$$\psi = \frac{(\Phi_{\psi} / \Delta T) - [U_f \times B_f] - \sum [U_{g,Bg}]}{B_g}$$

$$\psi = \frac{[47.8001 \text{ W/m}^2 / 20.00 \text{ °C}] - [2.3389 \text{ W/m}^2 \text{K} \times 0.0830 \text{ m}] - [5.8140 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [5.8140 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]}{0.380 \text{ m}}$$

Glazing transmittance Ug=5.81 W/m²K Frame transmittance Uf=2.34 W/m²K

Glazing size Bg: 380 mm

Frame size Bf: 83 mm

Simulation with glazing

Lg2D, with glazing:	2.3900 W/mK
Φψ, flow with glazing:	47.8001 W/m
Flow error:	0.000001
Triangles:	2080

Boundary conditions

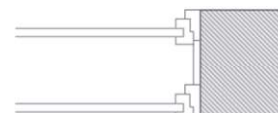
ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rai increased		20.000	0.2000	65.0

Boundary temperatures

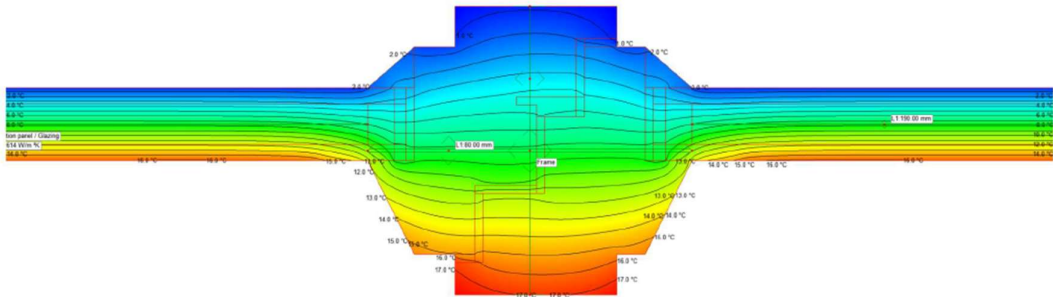
Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	397.00	4.283	17.004	6.201	42.1396
External	492.61	0.392	4.651	3.881	-47.8001
Adiabatic	4.00	4.651	4.884	4.767	-0.0000
Rai increased	118.70	3.982	17.004	10.463	5.6606

Name\λx [W/mK]	ε	Color
Glass 1.0000	0.900	
Putty 0.5000	0.900	
Larch 0.1300	0.900	
Air 0.0837	0.900	

Project:	Dante Schule	Detail:	Stulp aussen	File:	Stulp aussen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation ISO 10077-2 (2017) - radiosity	Transmittance Uf: 2.05 W/m²K
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Name	λx [W/mK]	ε	Color
EPDM	0.2500	0.900	
Box 2	0.6100	0.900	
Box 1	0.4000	0.900	
Glass	1.0000	0.900	
Larch	0.1300	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Putty	0.5000	0.900	
Argon	1.0433	0.900	
Argon	1.0433	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation
 $U_f = \frac{1}{\frac{1}{U_{f,2D}} + \frac{1}{U_{f,flow}}}$
 $U_f = \frac{1}{\frac{1}{25.9328 \text{ W/m}^2 \cdot \text{K}} + \frac{1}{20.00 \text{ °C}} - \frac{1}{2.8455 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}} - \frac{1}{2.8455 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}}} / 0.0800 \text{ m}$

Simulation with ISO10077 panel

Uf2D, with ISO10077 panel:	1.2966 W/mK
def. flow with ISO10077 panel:	25.9328 W/m
Flow error:	0.000000
Triangles:	4132

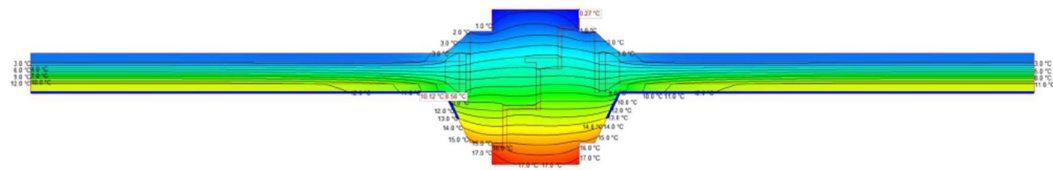
Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000

Project:	Dante Schule	Detail:	Stulp innen	File:	Stulp innen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation computation ISO 10077-2 (2017) - radiosity	Linear transmittance ψ: 0.051 W/mK Superficial condensation: 436 mm
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ψ computation

$$\psi = \frac{1}{\frac{1}{U_{f,2D}} + \frac{1}{U_{f,flow}}}$$

$$\psi = \frac{1}{\frac{1}{25.9328 \text{ W/m}^2 \cdot \text{K}} + \frac{1}{20.00 \text{ °C}} - \frac{1}{2.0483 \text{ W/m}^2 \cdot \text{K} \cdot 0.0800 \text{ m}} - \frac{1}{2.8455 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}} - \frac{1}{2.8455 \text{ W/m}^2 \cdot \text{K} \cdot 0.1900 \text{ m}}} / 0.0800 \text{ m}$$

Glazing transmittance Ug=2.85 W/m²K
 Frame transmittance Uf=2.05 W/m²K
 Glazing size Bg: 380 mm
 Frame size Bf: 80 mm

Simulation with glazing

Uf2D, with glazing:	1.2966 W/mK
Φψ, flow with glazing:	25.9328 W/m
Flow error:	0.000000
Triangles:	4132

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0

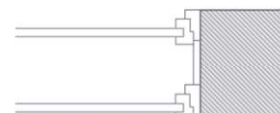
Boundary temperatures

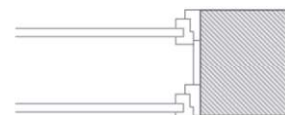
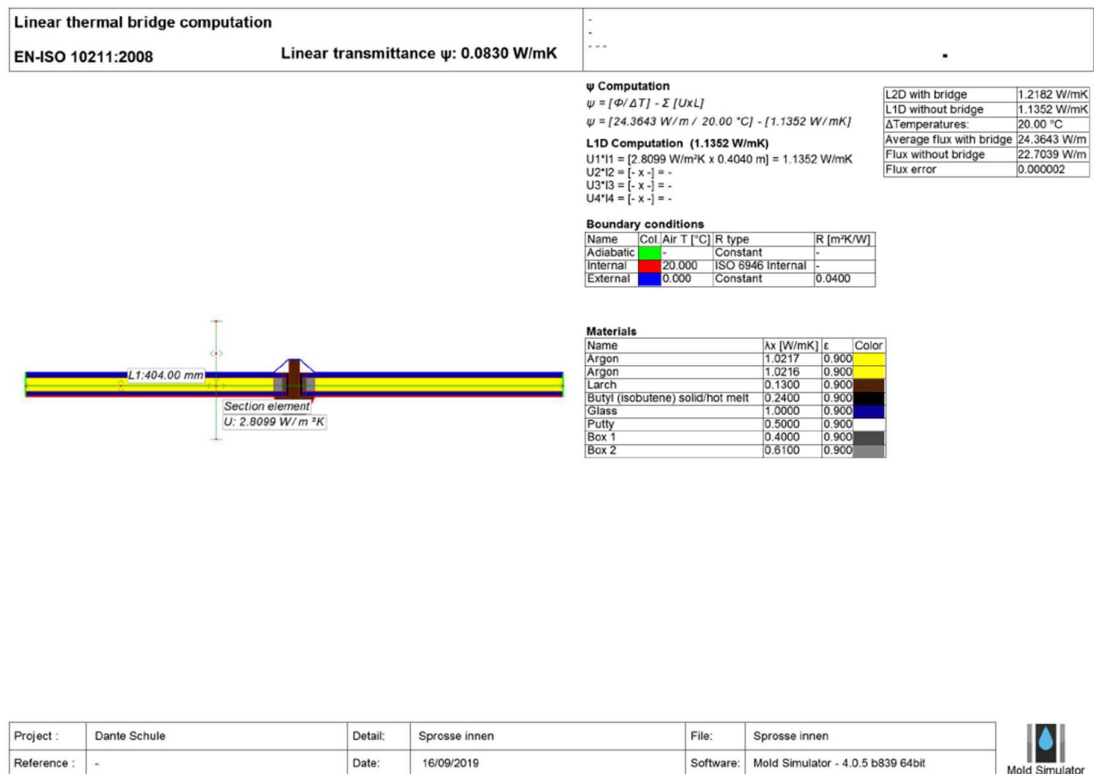
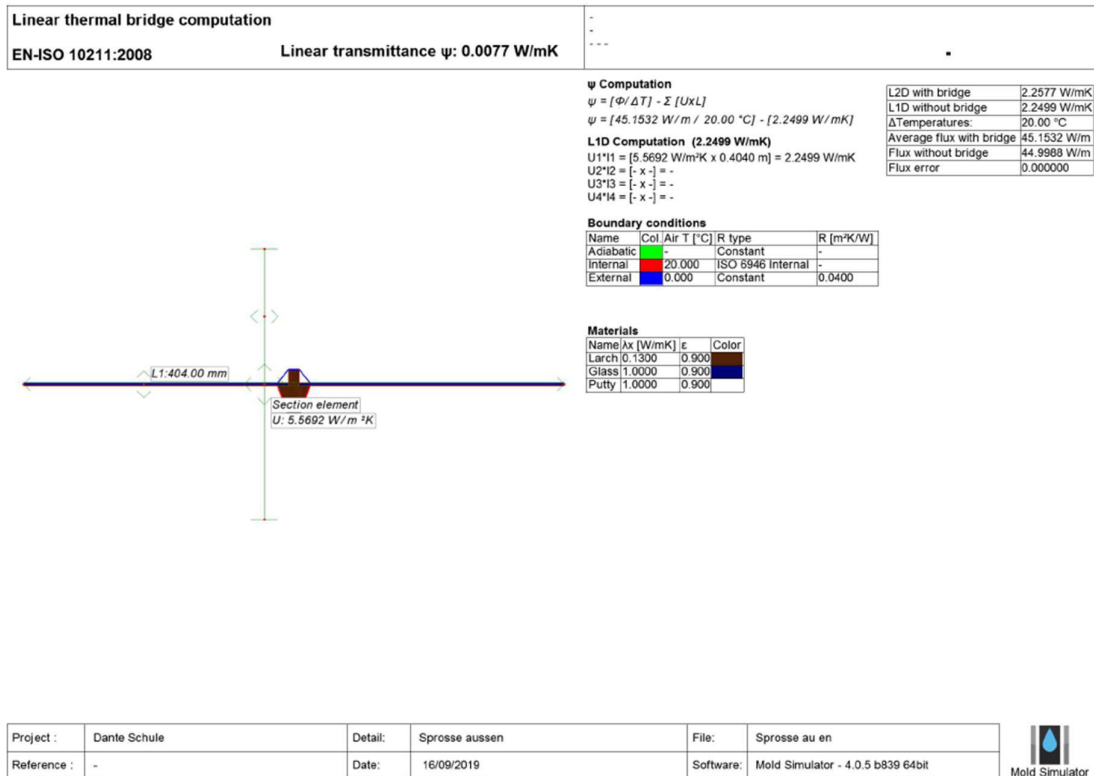
Name	L [mm]	Min T [°C]	Max T [°C]	Avg T [°C]	Q [W/m]
Internal	397.00	10.121	17.768	12.767	22.0880
External	487.48	0.274	3.663	2.128	-25.9328
Adiabatic	36.00	2.274	12.596	7.434	0.0000
Rsi increased	111.43	8.578	17.768	13.099	3.8447

Name	λx [W/mK]	ε	Color
EPDM	0.2500	0.900	
Box 2	0.6100	0.900	
Box 1	0.4000	0.900	
Glass	1.0000	0.900	
Larch	0.1300	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Putty	0.5000	0.900	
Argon	1.0433	0.900	
Argon	1.0433	0.900	

Name	λx [W/mK]	ε	Color
10077 radiosity	-	0.900	

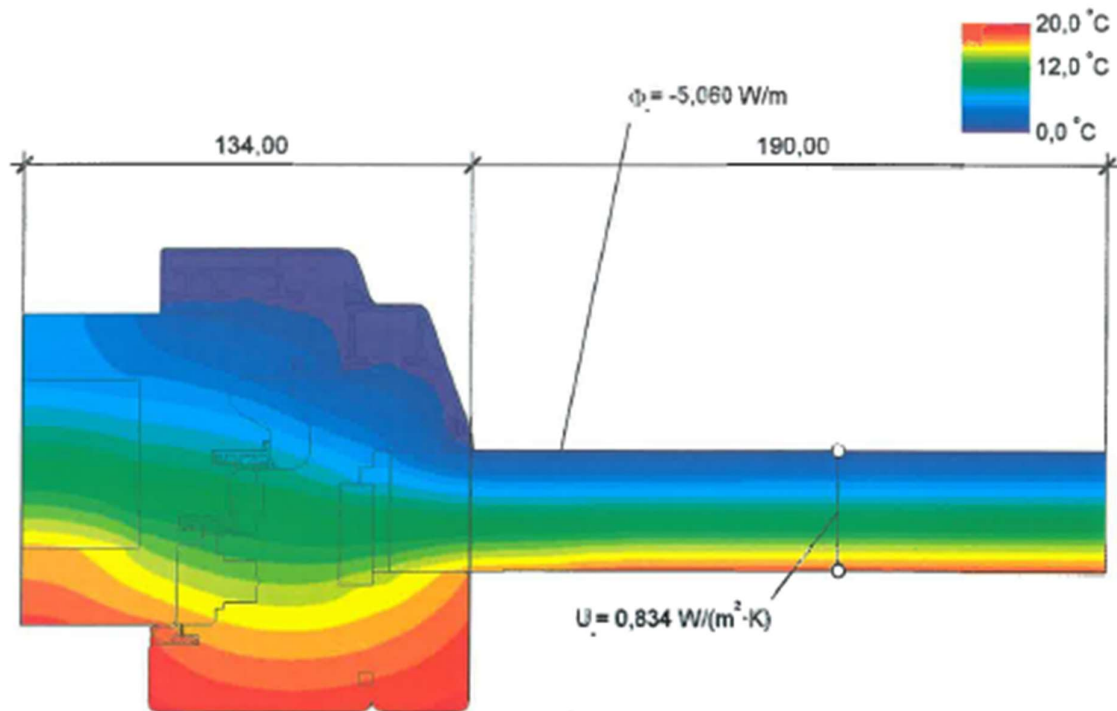
Project:	Dante Schule	Detail:	Stulp innen	File:	Stulp innen
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



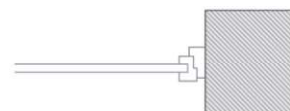


Austausch Fensterkonstruktion (Einfachfenster)

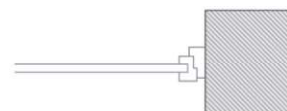
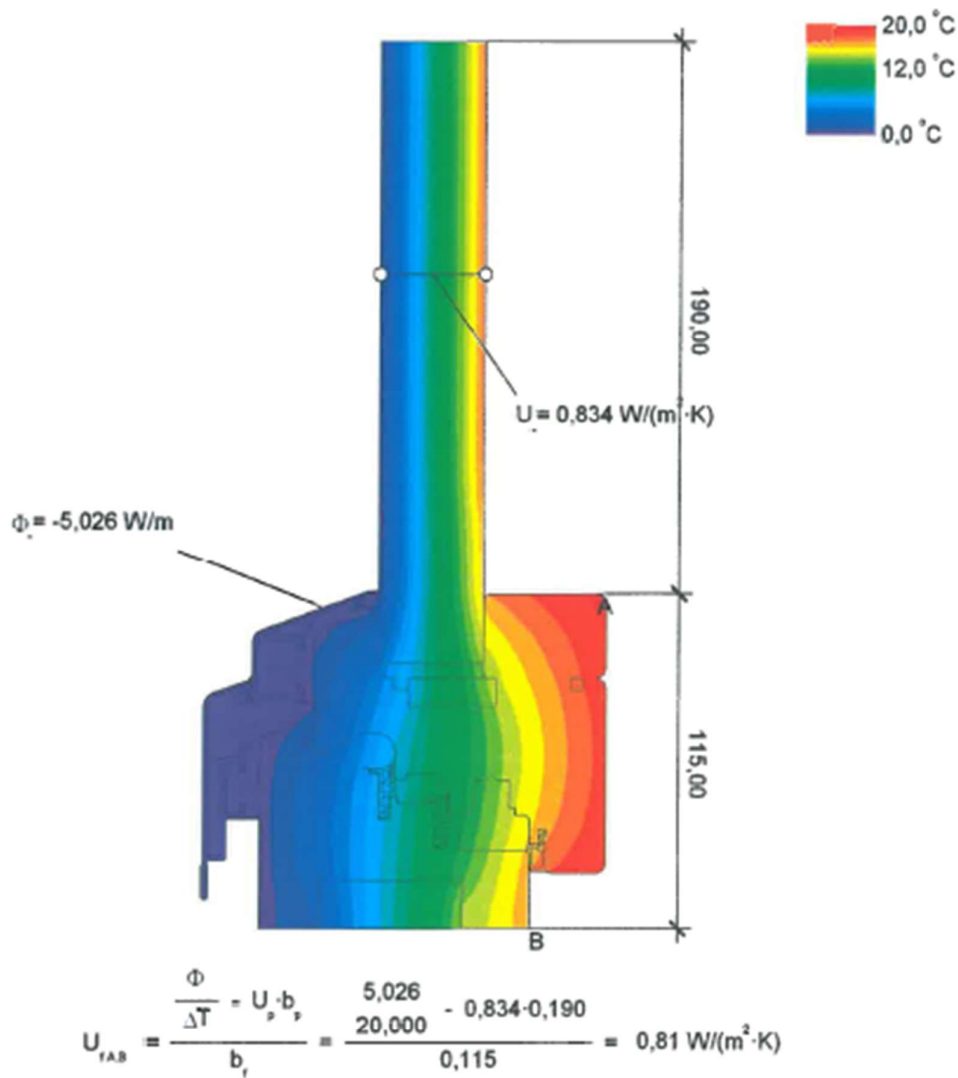
$U_{f1} \lambda=0,11 \text{ W/mK}$
Nodo laterale/superiore



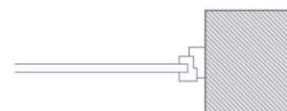
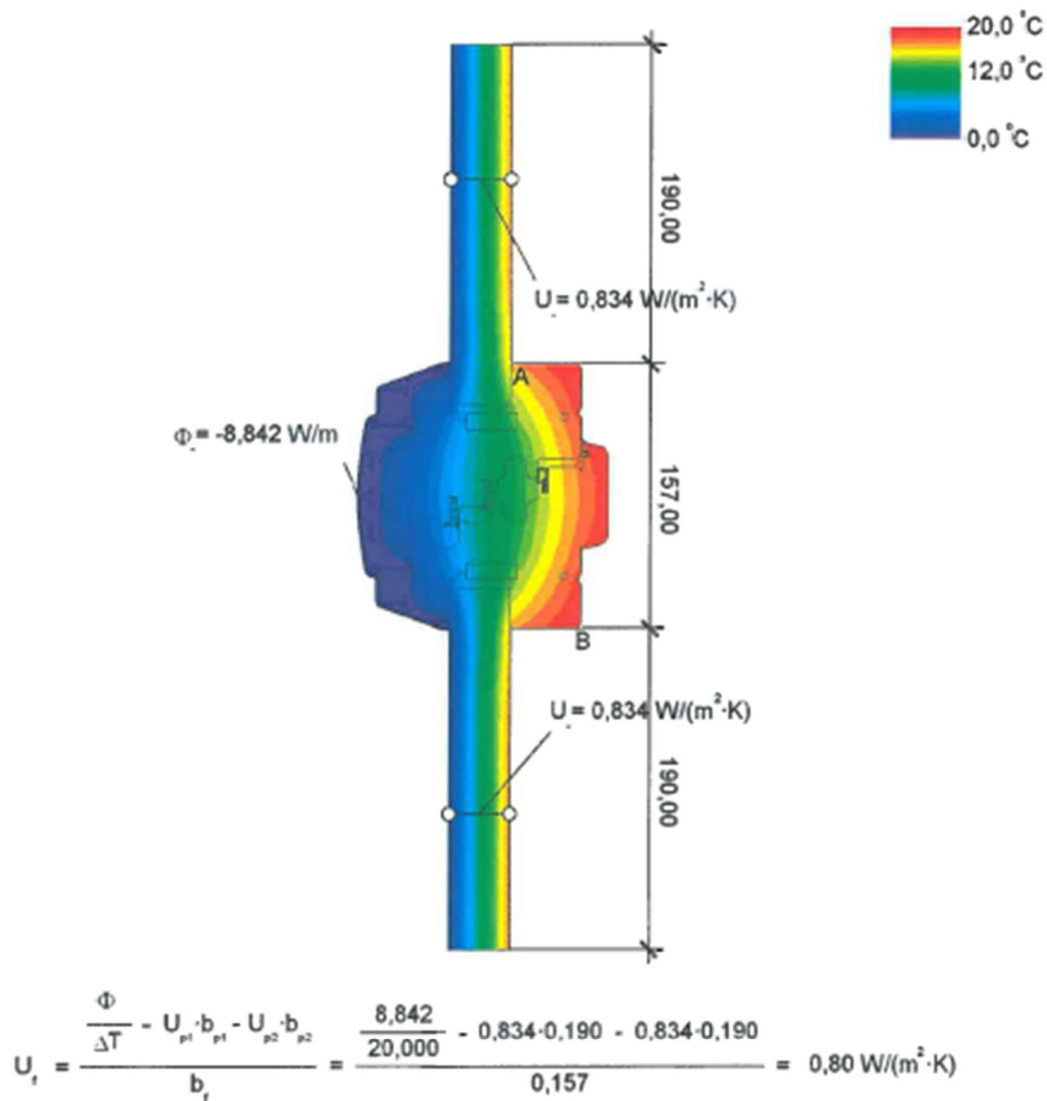
$$U_f = \frac{\frac{\Phi}{\Delta T} - U_p \cdot b_p}{b_f} = \frac{\frac{5,060}{20,000} - 0,834 \cdot 0,190}{0,134} = 0,70 \text{ W/(m}^2 \cdot \text{K)}$$



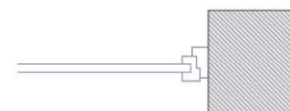
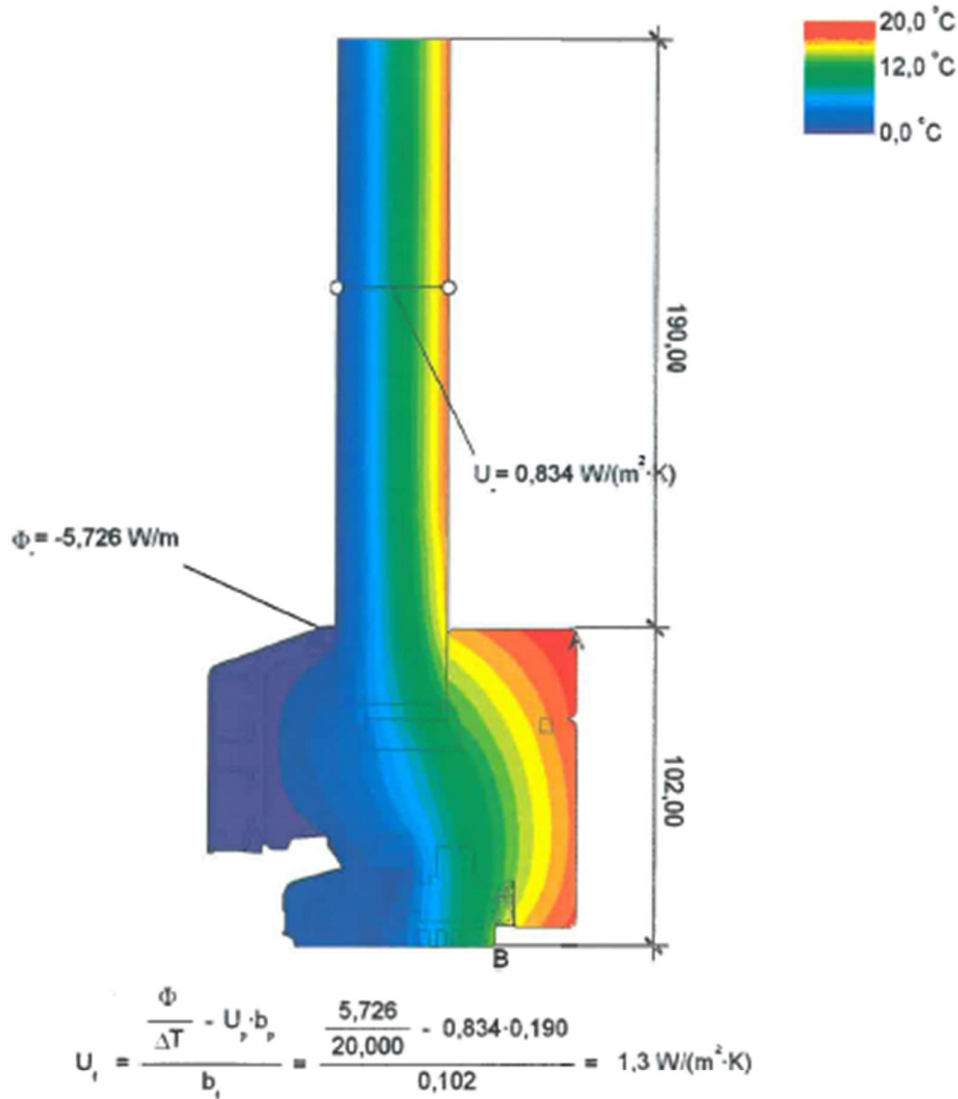
$U_{f2} \lambda=0,11 \text{ W/mK}$
Nodo inferiore finestra



$U_{f3} \lambda=0,11 \text{ W/mK}$
Nodo centrale

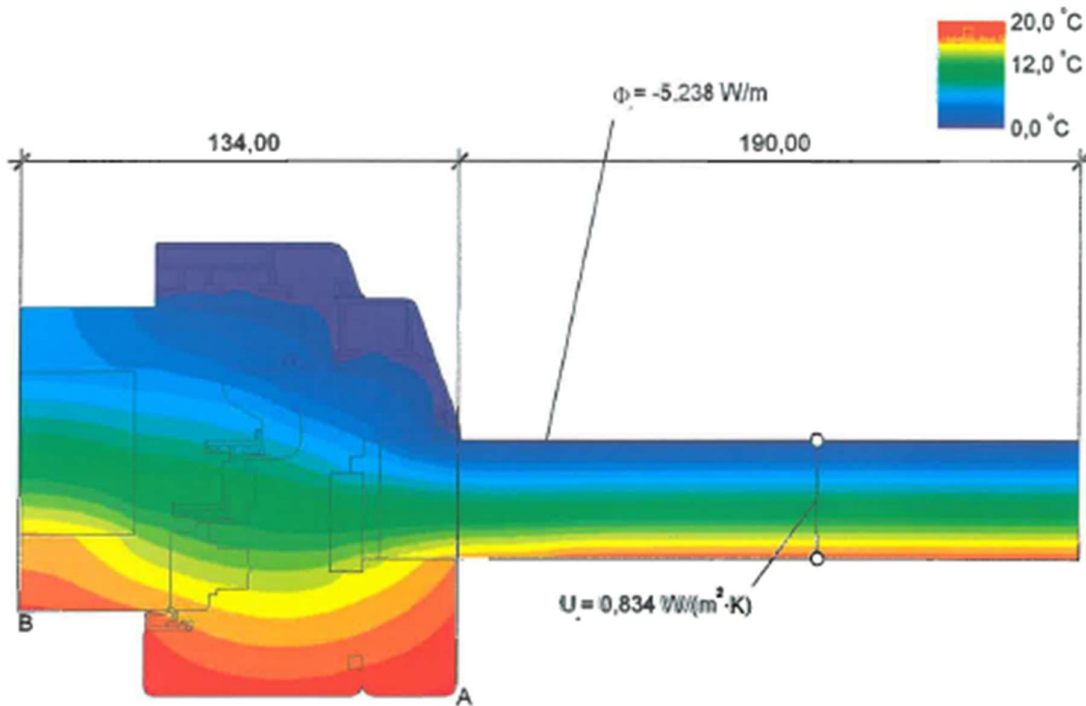


$U_{f4} \lambda=0,11 \text{ W/mK}$
Nodo inferiore portafinestra

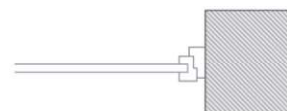


$$U_{1,3} = \frac{\frac{\Phi}{\Delta T} - U_{p1} \cdot b_{p1} - U_{p2} \cdot b_{p2}}{b_1} = \frac{\frac{8,011}{20,000} - 0,834 \cdot 0,190 - 0,834 \cdot 0,190}{0,094} = 0,89 \text{ W/(m}^2 \cdot \text{K)}$$

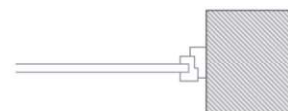
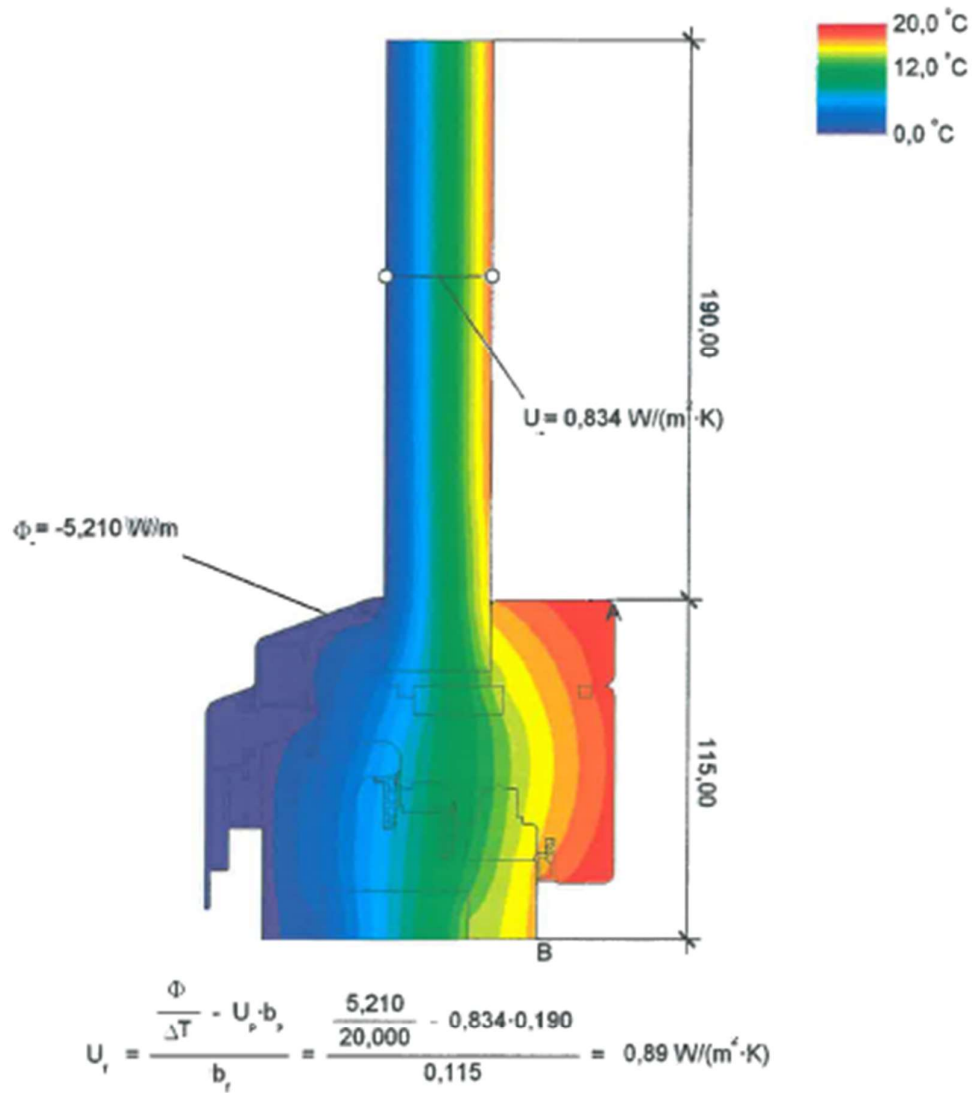

$U_{f1} \lambda=0,13 \text{ W/mK}$
Nodo laterale/superiore



$$U_f = \frac{\frac{\phi}{\Delta T} - U_p \cdot b_p}{b_f} = \frac{\frac{5,238}{20,000} - 0,834 \cdot 0,190}{0,134} = 0,77 \text{ W/(m}^2 \cdot \text{K)}$$

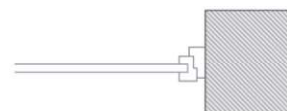
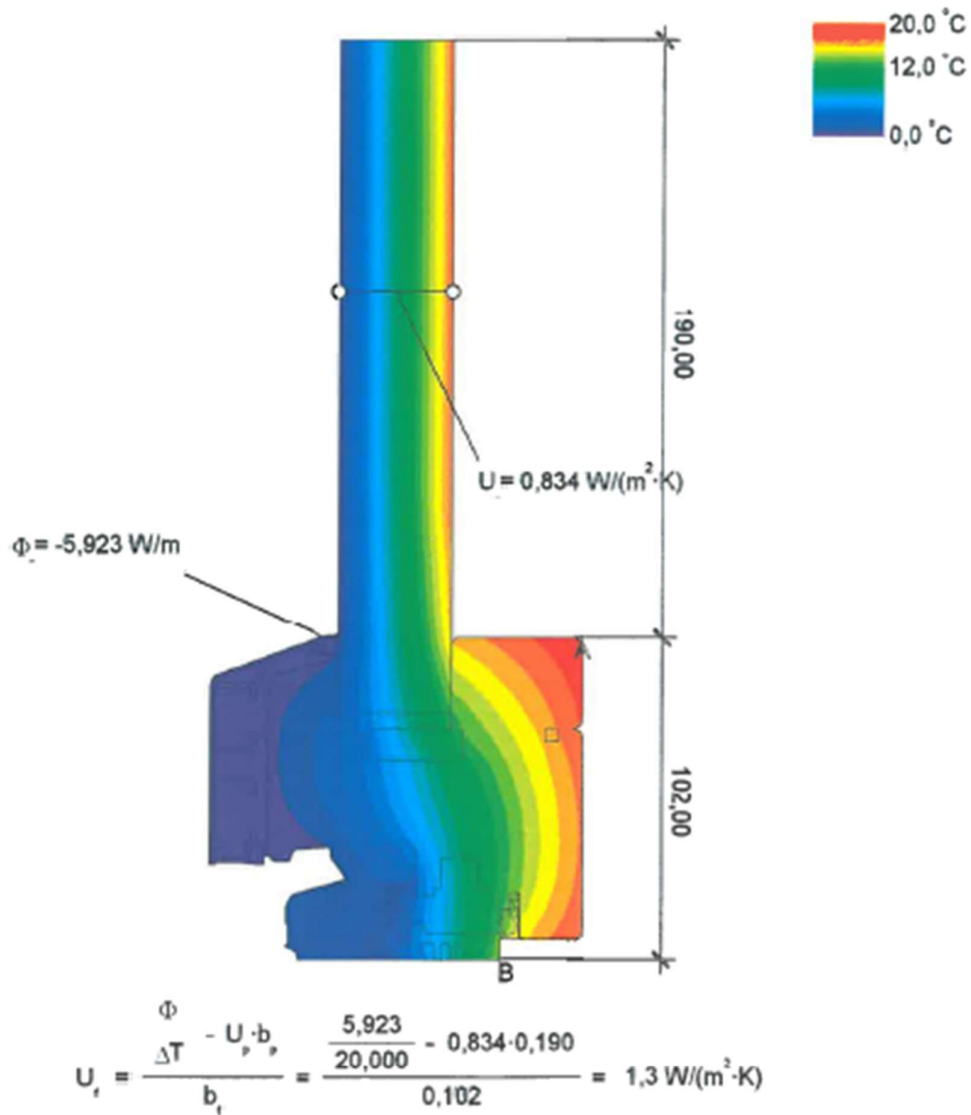


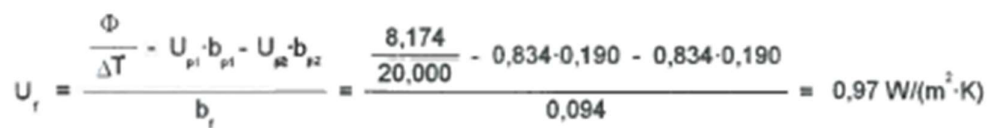
$U_{f2} \lambda = 0,13 \text{ W/mK}$
Nodo inferiore finestra



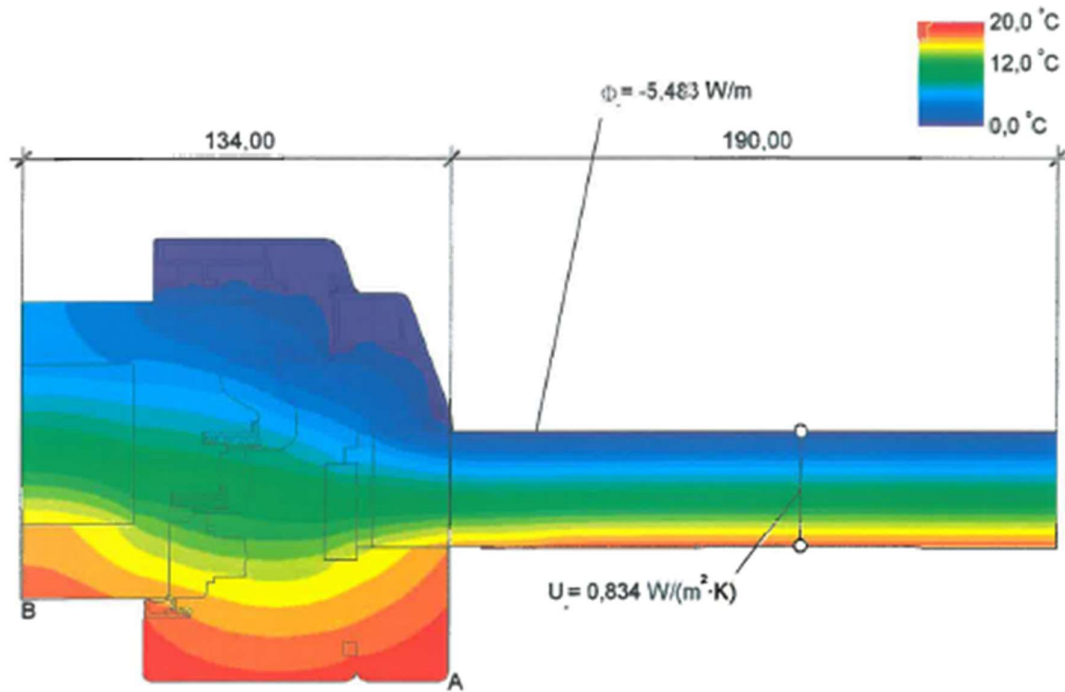
$$U_{fA,B} = \frac{\frac{\Phi}{\Delta T} - U_{p1} \cdot b_{p1} - U_{p2} \cdot b_{p2}}{b_f} = \frac{\frac{9,085}{20,000} - 0,834 \cdot 0,190 - 0,834 \cdot 0,190}{0,157} = 0,87 \text{ W/(m}^2 \cdot \text{K)}$$


$U_{f4} \lambda=0,13 \text{ W/mK}$
Nodo inferiore portafinestra

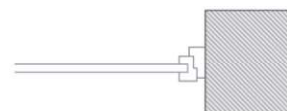




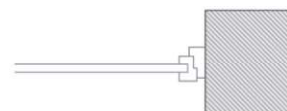
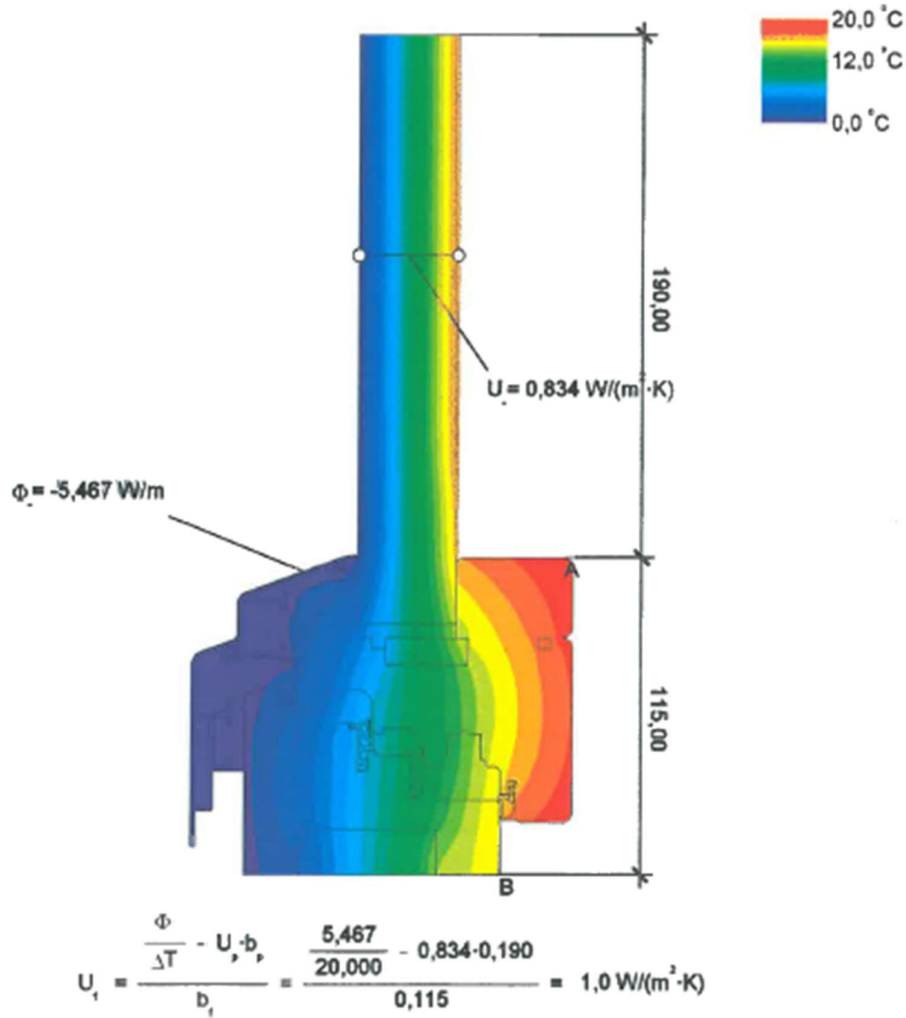
$U_{f1} \lambda=0,16 \text{ W/mK}$
Nodo laterale/superiore



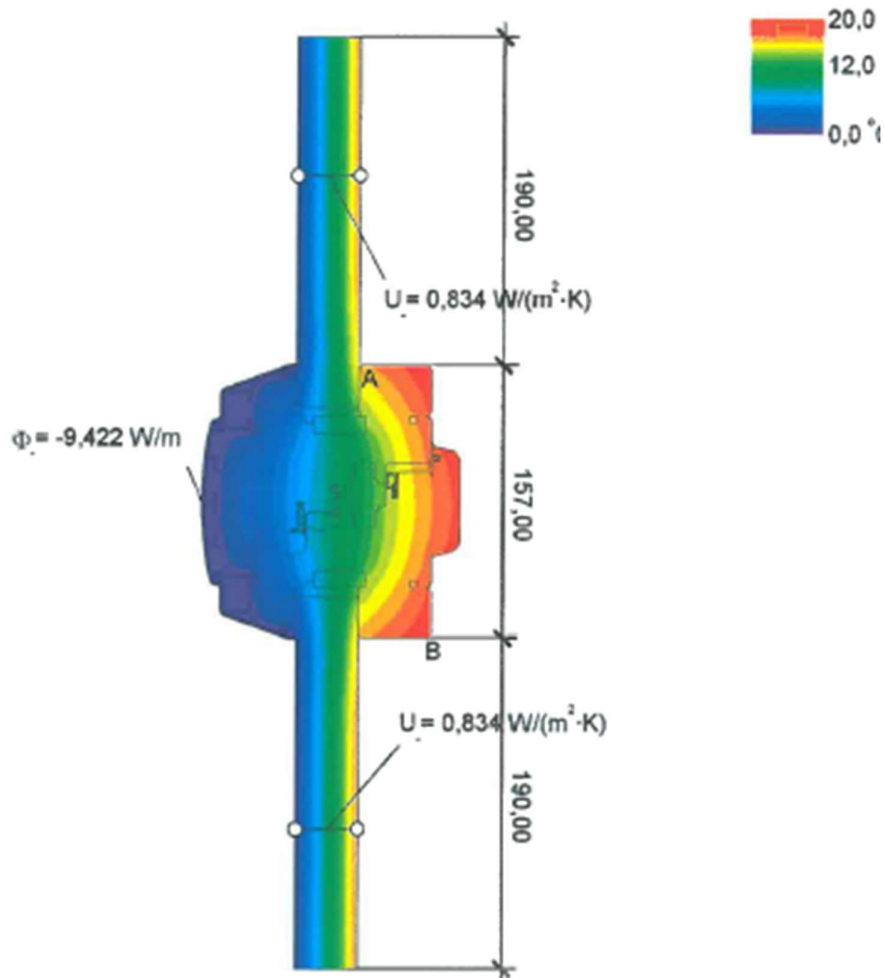
$$U_f = \frac{\frac{\Phi}{\Delta T} - U_s \cdot b_s}{b_f} = \frac{\frac{5,483}{20,000} - 0,834 \cdot 0,190}{0,134} = 0,86 \text{ W/(m}^2 \cdot \text{K)}$$



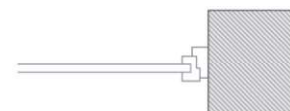
$U_{f2} \lambda=0,16 \text{ W/mK}$
Nodo inferiore finestra



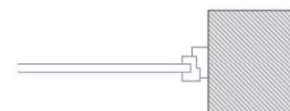
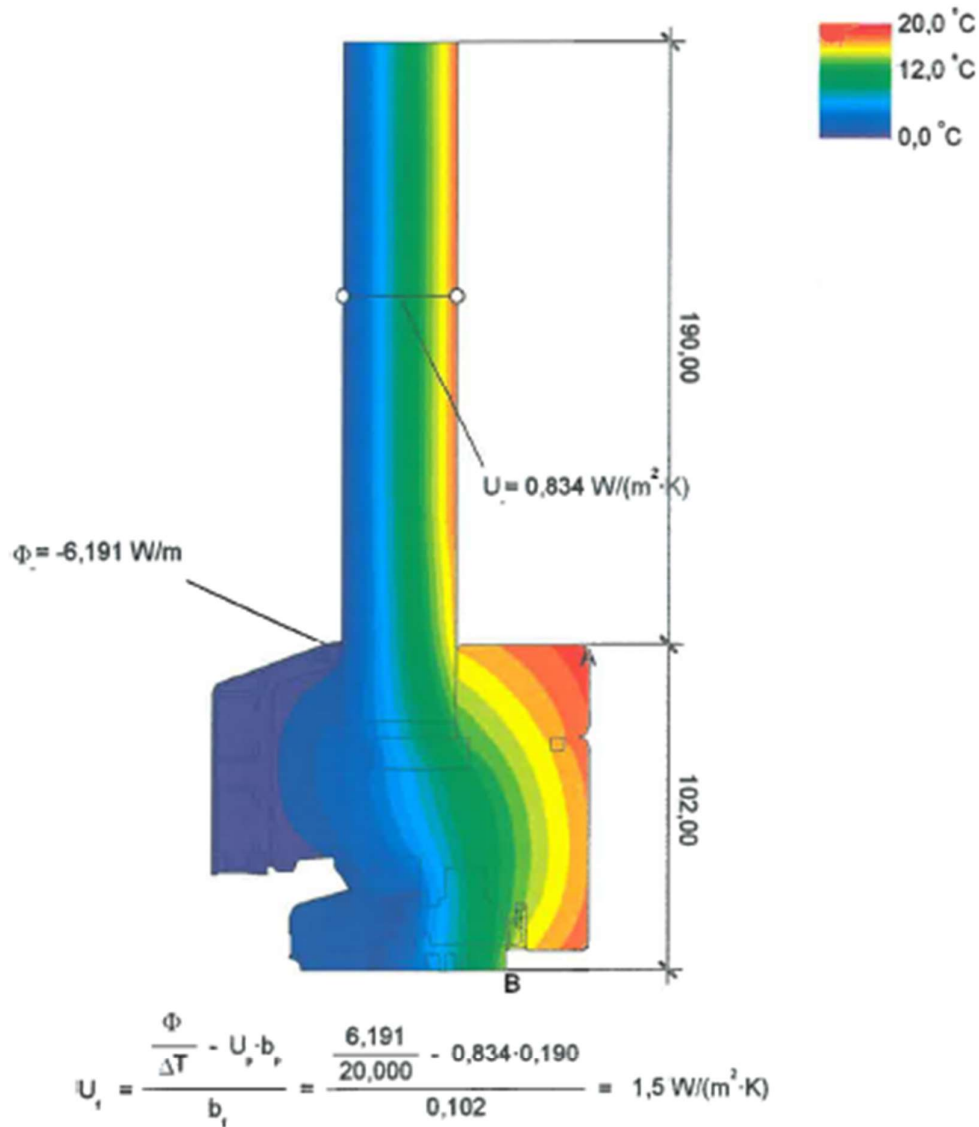
$U_{f3} \lambda=0,16 \text{ W/mK}$
Nodo centrale



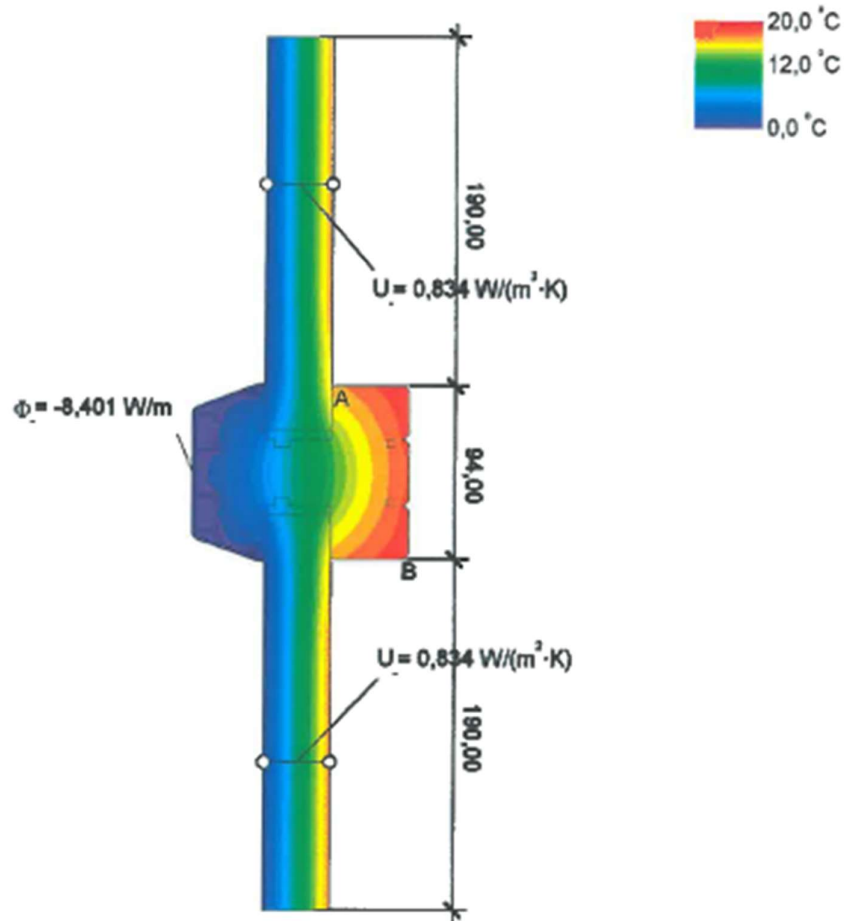
$$U_f = \frac{\frac{\Phi}{\Delta T} - U_{f1} \cdot b_{f1} - U_{f2} \cdot b_{f2}}{b_f} = \frac{\frac{9,422}{20,000} - 0,834 \cdot 0,190 - 0,834 \cdot 0,190}{0,157} = 0,98 \text{ W/(m}^2 \cdot \text{K)}$$



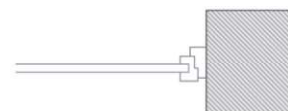
$U_{f4} \lambda=0,16 \text{ W/mK}$
Nodo inferiore portafinestra



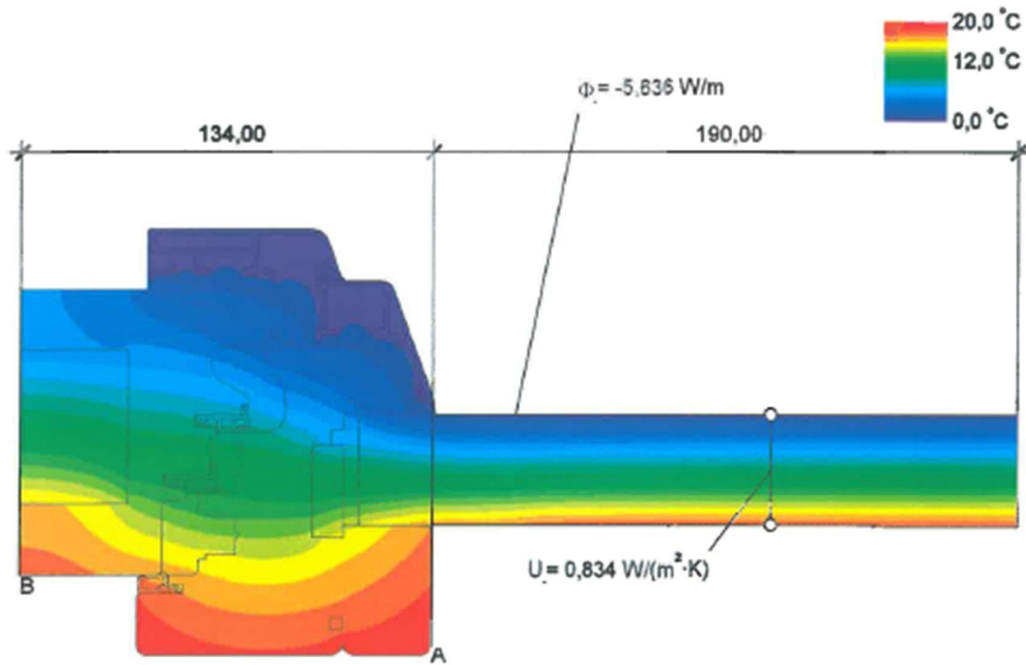
$U_{f5} \lambda = 0,16 \text{ W/mK}$
Nodo traversa rompitratta



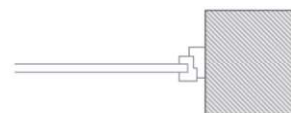
$$U_f = \frac{\frac{\Phi}{\Delta T} - U_{p1} \cdot b_{p1} - U_{p2} \cdot b_{p2}}{b_f} = \frac{\frac{8,401}{20,000} - 0,834 \cdot 0,190 - 0,834 \cdot 0,190}{0,094} = 1,1 \text{ W/(m}^2 \cdot \text{K)}$$



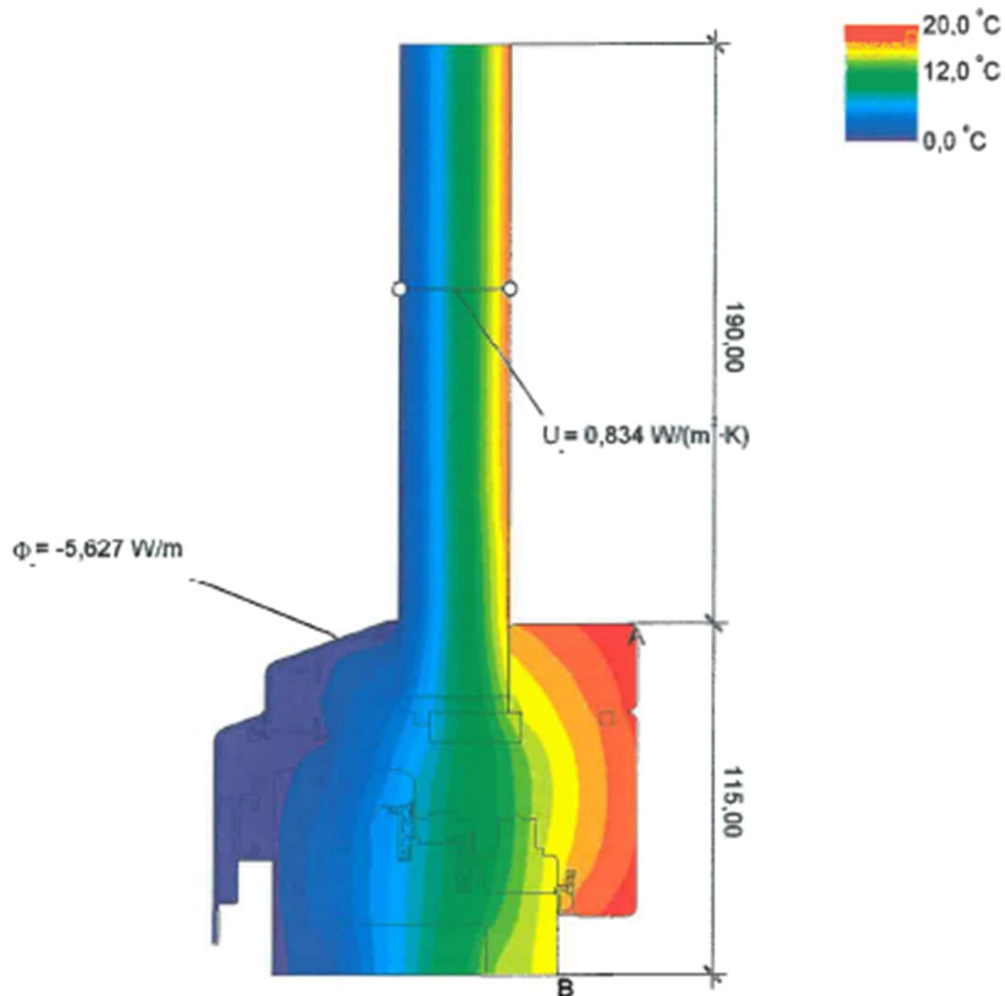
$U_{f1} \lambda=0,18 \text{ W/mK}$
Nodo laterale/superiore



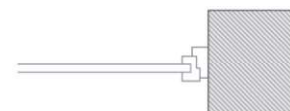
$$U_f = \frac{\frac{\Phi}{\Delta T} - U_p \cdot b_p}{b_f} = \frac{\frac{5,636}{20,000} - 0,834 \cdot 0,190}{0,134} = 0,92 \text{ W/(m}^2 \cdot \text{K)}$$



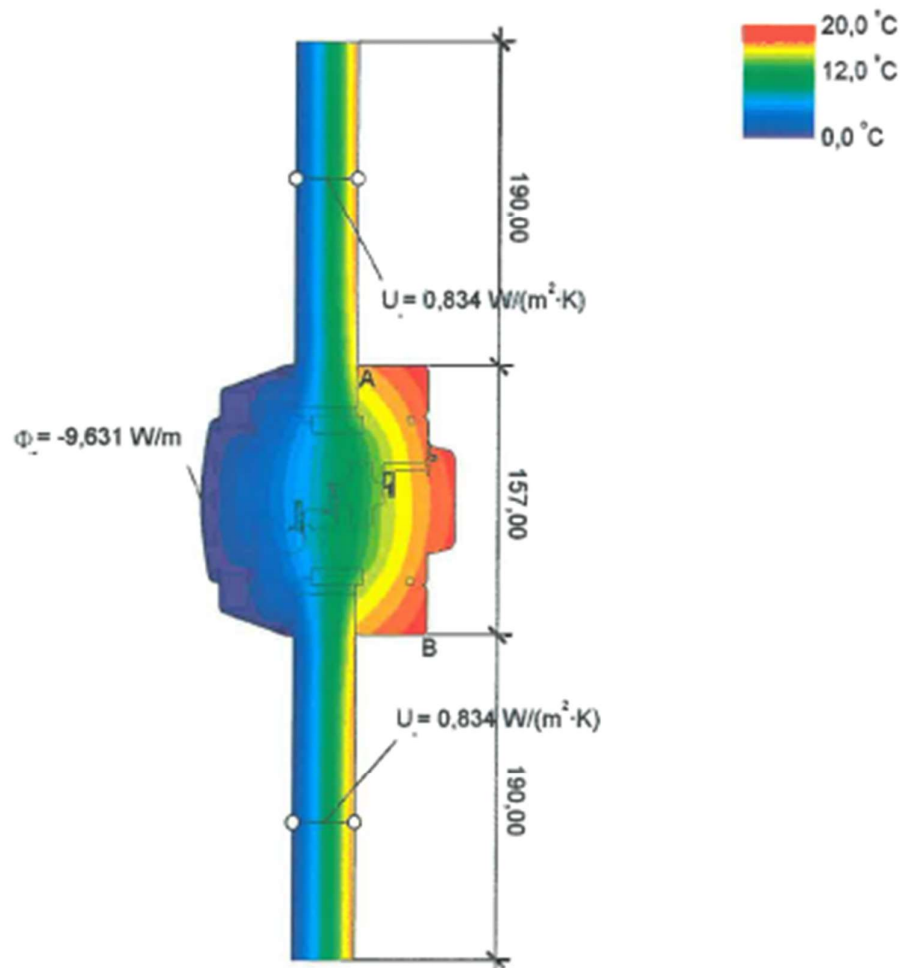
$U_{f2} \lambda=0,18 \text{ W/mK}$
Nodo inferiore finestra



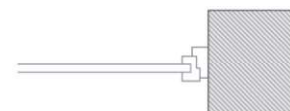
$$U_t = \frac{\frac{\Phi}{\Delta T} - U \cdot b_t}{b_t} = \frac{\frac{5,627}{20,000} - 0,834 \cdot 0,190}{0,115} = 1,1 \text{ W/(m}^2 \cdot \text{K)}$$



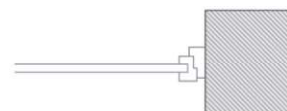
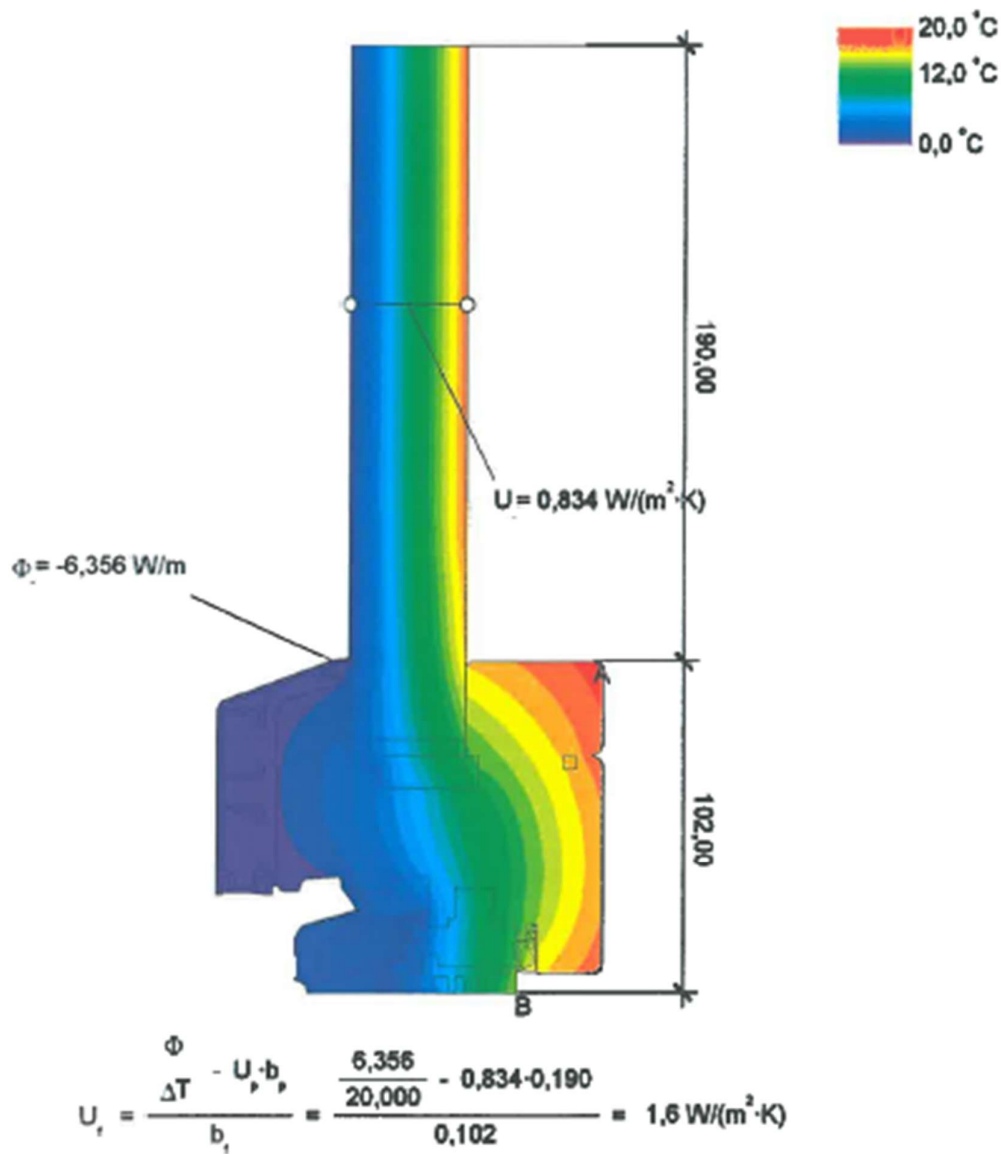
$U_{f3} \lambda = 0,18 \text{ W/mK}$
Nodo centrale



$$U_f = \frac{\frac{\Phi}{\Delta T} - U_{p1} \cdot b_{p1} - U_{p2} \cdot b_{p2}}{b_f} = \frac{\frac{9,631}{20,000} - 0,834 \cdot 0,190 - 0,834 \cdot 0,190}{0,157} = 1,0 \text{ W/(m}^2 \cdot \text{K)}$$



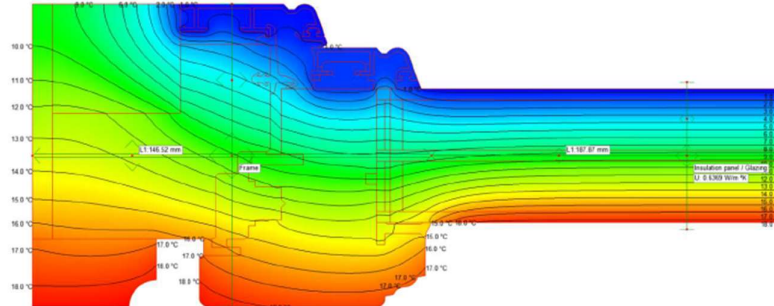
$U_{f4} \lambda=0,18 \text{ W/mK}$
Nodo inferiore portafinestra



Austausch Fensterkonstruktion (Einfachfenster)

Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.05 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Box 2	0.6100	0.900	
Box 1	0.4000	0.900	
Glass	1.0000	0.900	
Argon	1.0380	0.900	
Argon	1.0970	0.900	
Larch	0.1300	0.900	
Aluminium (anodized/coated)	160.0000	0.900	
PVC flexible	0.1400	0.900	
Steel	50.0000	0.900	
Polyurethane high density	0.0400	0.900	
EPDM	0.2500	0.900	
Silicone	1.0000	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \left(\frac{\Phi_f}{\Delta T} \right) - \sum \left(U_{x,Bp} \right) / B_f$$

$$U_f = \left(\frac{10.0967 \text{ W/m}^2 / 20.00 \text{ °C}}{1.7272 \text{ W/m}^2 \text{K} \times 0.1879 \text{ m}} \right) - \left(\frac{0.1465 \text{ m}}{1.7272 \text{ W/m}^2 \text{K}} \right)$$

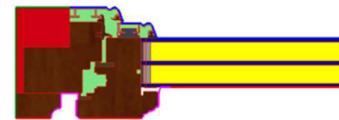
Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	0.5048 W/mK
Φf, flow with ISO10077 panel:	10.0967 W/m
Flow error:	0.000001
Triangles:	13146

Frame width Bf: 146.52 mm Panel width Bp: 187.87 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal	20.000	0.1300	0.0400
External	0.000	-	-
Adiabatic	20.000	0.2000	-
Rsi increased	20.000	0.2000	-

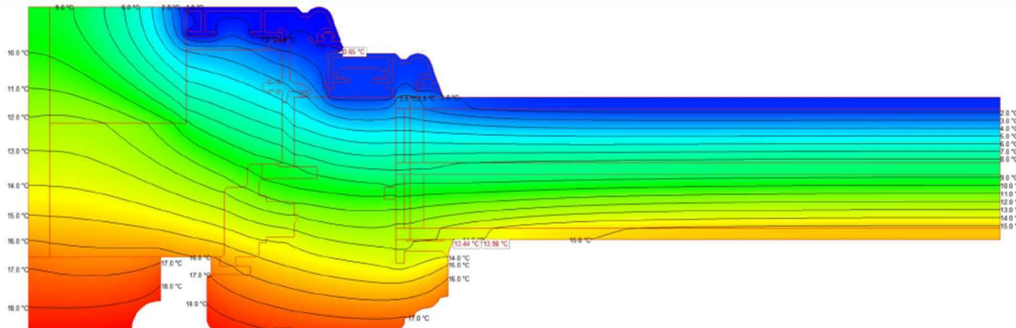


Project:	Villa Castelli	Detail:	Rahmen l,r.o mit Aluminiumverkleidung	File:	Rahmen o,l,r
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation comput
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.026 W/mK
Superficial condensation: 0 mm



ψ computation

$$\psi = \left(\frac{\Phi_{\psi}}{\Delta T} \right) - \sum \left(U_{x,Bp} \right) / B_{\psi}$$

$$\psi = \left(\frac{10.0967 \text{ W/m}^2 / 20.00 \text{ °C}}{1.0513 \text{ W/m}^2 \text{K} \times 0.1465 \text{ m}} \right) - \left(\frac{1.7272 \text{ W/m}^2 \text{K} \times 0.1879 \text{ m}}{1.0513 \text{ W/m}^2 \text{K}} \right)$$

Simulation with glazing

Lf2D, with glazing:	0.5048 W/mK
Φψ, flow with glazing:	10.0967 W/m
Flow error:	0.000001
Triangles:	13146

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal	20.000	0.1300	65.0	
1	External	0.000	0.0400	65.0	
2	Adiabatic	-	-	65.0	
3	Rsi increased	20.000	0.2000	65.0	

Materials

Name	λx [W/mK]	ε	Color
Box 2	0.6100	0.900	
Box 1	0.4000	0.900	
Glass	1.0000	0.900	
Argon	1.0380	0.900	
Argon	1.0970	0.900	
Larch	0.1300	0.900	
Aluminium (anodized/coated)	160.0000	0.900	
PVC flexible	0.1400	0.900	
Steel	50.0000	0.900	

Name	λx [W/mK]	ε	Color
Polyurethane high density	0.0400	0.900	
EPDM	0.2500	0.900	
Silicone	1.0000	0.900	
10077 radiosity	-	0.900	

Glazing transmittance Ug=1.73 W/m²K

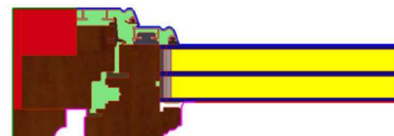
Glazing size Bg: 188 mm

Frame transmittance Uf=1.05 W/m²K

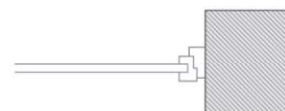
Frame size Bf: 147 mm

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	275.01	13.981	18.854	16.236	7.9626
External	306.94	0.650	2.274	1.316	-10.0967
Adiabatic	214.39	0.831	18.621	10.798	-0.0029
Rsi increased	129.45	13.436	18.854	16.703	2.1341

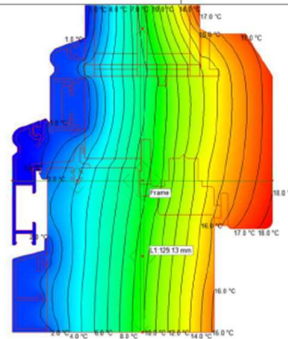


Project:	Villa Castelli	Detail:	Rahmen l,r.o mit Aluminiumverkleidung	File:	Rahmen o,l,r
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Frame Uf computation ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.32 W/m²K



Materials

Name	λx [W/mK]	ε	Color
EPDM	0.2500	0.900	
PVC flexible	0.1400	0.900	
Aluminium (anodized/coated)	160.0000	0.900	
Steel	50.0000	0.900	
Argon	0.0906	0.900	
Larch	0.0960	0.900	
Silicone	0.5000	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = \left(\frac{\Phi_f}{\Delta T} \right) - \sum \left(U_{x,Bp} \right) / B_f$$

$$U_f = \left(\frac{10.4327 \text{ W/m}^2 / 20.00 \text{ °C}}{1.7269 \text{ W/m}^2 \cdot \text{K} \times 0.1879 \text{ m}} \right) - \left(\frac{1.12913 \text{ m}}{0.1291 \text{ m}} \right)$$

Simulation with ISO10077 panel

L12D, with ISO10077 panel:	0.5216 W/mK
Φf, flow with ISO10077 panel:	10.4327 W/m
Flow error:	0.000000
Triangles:	13203

Frame width Bf: 129.13 mm Panel width Bp: 187.87 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic		-	-
Rsi increased		20.000	0.2000
Rs external cavities		0.000	0.3000



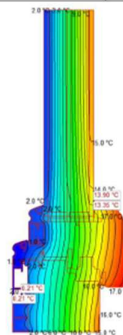
Project:	Villa Castelli	Detail:	Rahmen u mit Aluminiumverkleidung	File:	Rahmen u
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



ψ and condensation comput ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.027 W/mK

Superficial condensation: 0 mm



ψ computation

$$\psi = \left(\frac{\Phi_{\psi}}{\Delta T} \right) - \sum \left(U_{gxBg} \right)$$

$$\psi = \left(\frac{10.4327 \text{ W/m}^2 / 20.00 \text{ °C}}{1.3179 \text{ W/m}^2 \cdot \text{K} \times 0.1291 \text{ m}} \right) - \left(\frac{1.7269 \text{ W/m}^2 \cdot \text{K} \times 0.1879 \text{ m}}{1.12913 \text{ m}} \right)$$

Simulation with glazing

L12D, with glazing:	0.5216 W/mK
Φψ, flow with glazing:	10.4327 W/m
Flow error:	0.000000
Triangles:	13203

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Rsi increased		20.000	0.2000	65.0
5	Rs external cavities		0.000	0.3000	65.0

Materials

Name	λx [W/mK]	ε	Color
EPDM	0.2500	0.900	
PVC flexible	0.1400	0.900	
Aluminium (anodized/coated)	160.0000	0.900	
Steel	50.0000	0.900	
Argon	0.0906	0.900	
Larch	0.0960	0.900	
Silicone	0.5000	0.900	
Glass	1.0000	0.900	

Name	λx [W/mK]	ε	Color
Box 1	0.4000	0.900	
Box 2	0.6100	0.900	
10077 radiosity	-	0.900	

Glazing transmittance Ug=1.73 W/m²K Frame transmittance Uf=1.32 W/m²K

Glazing size Bg: 188 mm

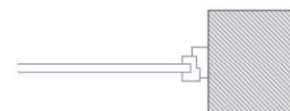
Frame size Bf: 129 mm

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	261.99	13.900	18.296	15.844	8.3754
External	337.83	0.206	2.218	1.185	-10.0102
Adiabatic	134.99	1.281	16.205	7.934	0.0093
Rsi increased	102.17	13.348	18.296	15.973	2.0573
Rs external cavities	140.17	0.205	2.924	0.904	-0.4225



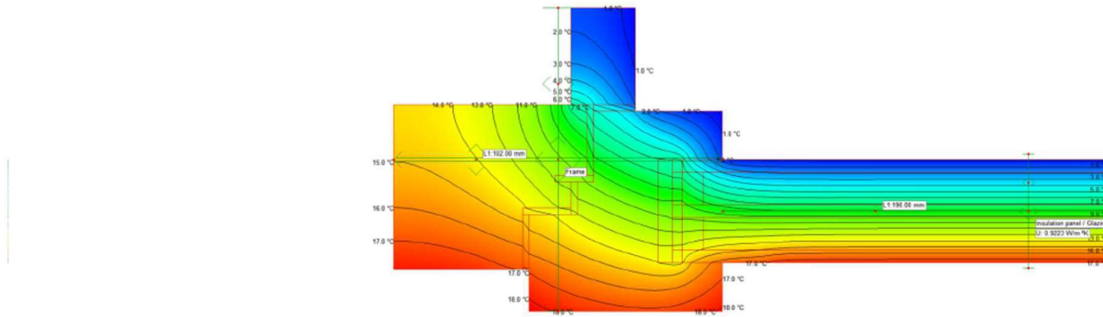
Project:	Villa Castelli	Detail:	Rahmen u mit Aluminiumverkleidung	File:	Rahmen u
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



Austausch Fensterkonstruktion (Einfachfenster)

Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.04 W/m²K



Materials

Name	λx [W/mK]	ε	Color
Larch	0.1300	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
EPDM	0.2500	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 1	0.6100	0.900	
Argon	1.0242	0.900	
Argon	1.0709	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

$$U_f = ([\Phi_f / \Delta T] - \Sigma [U_{x,Bp}]) / B_f$$

$$U_f = ([10.1291 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.9012 \text{ W/m}^2 \times 0.1900 \text{ m}] - [x]) / 0.1020 \text{ m}$$

Simulation with ISO10077 panel

Lf2D, with ISO10077 panel:	0.5065 W/mK
Φf, flow with ISO10077 panel:	10.1291 W/m
Flow error:	0.000010
Triangles:	4691

Frame width Bf: 102.00 mm Panel width Bp: 190.00 mm

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic			
Rsi increased		20.000	0.2000
Rs external cavities		0.000	0.3000

Project: Villa Tribus

Detail: Rahmen I,r,u

File: Rahem I,r,o

Client: -

Date: 22/09/2019

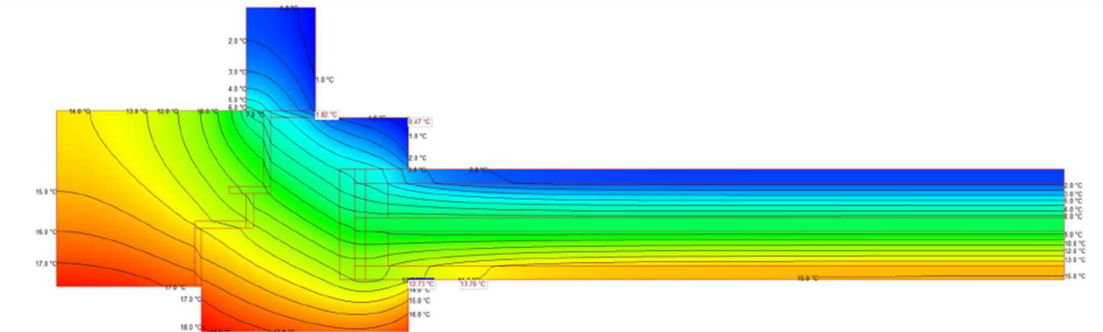
Software: Frame Simulator - 4.0.5 b839 64bit



ψ and condensation comput
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ: 0.039 W/mK

Superficial condensation: 9 mm



ψ computation

$$\psi = [\Phi_{\psi} / \Delta T] - [U_f \times B_f] - \Sigma [U_{g,x} B_g]$$

$$\psi = [10.1291 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.0412 \text{ W/m}^2 \times 0.1020 \text{ m}] - [1.9012 \text{ W/m}^2 \times 0.1900 \text{ m}] - [x]$$

Simulation with glazing

Lf2D, with glazing:	0.5065 W/mK
Φψ, flow with glazing:	10.1291 W/m
Flow error:	0.000010
Triangles:	4691

Boundary conditions

ID/Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0 Internal		20.000	0.1300	65.0
1 External		0.000	0.0400	65.0
2 Adiabatic				65.0
3 Rsi increased		20.000	0.2000	65.0
5 Rs external cavities		0.000	0.3000	65.0

Materials

Name	λx [W/mK]	ε	Color
Larch	0.1300	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
EPDM	0.2500	0.900	
Glass	1.0000	0.900	
Box 1	0.4000	0.900	
Box 1	0.6100	0.900	
Argon	1.0242	0.900	
Argon	1.0709	0.900	
10077 radiosity	-	0.900	

Glazing transmittance Ug=1.90 W/m²K

Glazing size Bg: 190 mm

Frame transmittance Uf=1.04 W/m²K

Frame size Bf: 102 mm

Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	264.00	13.696	18.158	15.622	8.8907
External	269.87	0.473	3.599	1.553	-10.0904
Adiabatic	187.87	0.521	17.942	9.812	0.0136
Rsi increased	56.00	12.729	18.158	15.578	1.2383
Rs external cavities	4.00	1.821	3.473	2.906	-0.0387

Project: Villa Tribus

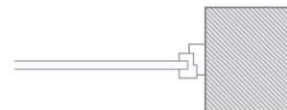
Detail: Rahmen I,r,u

File: Rahem I,r,o

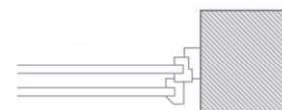
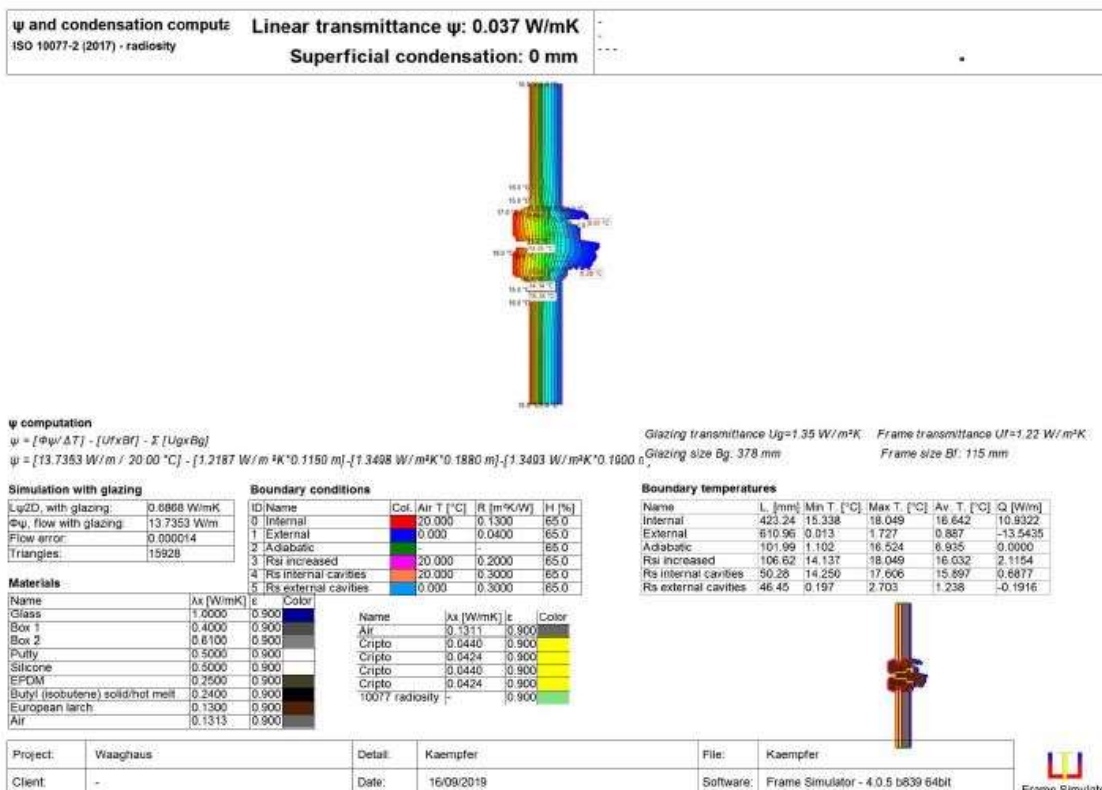
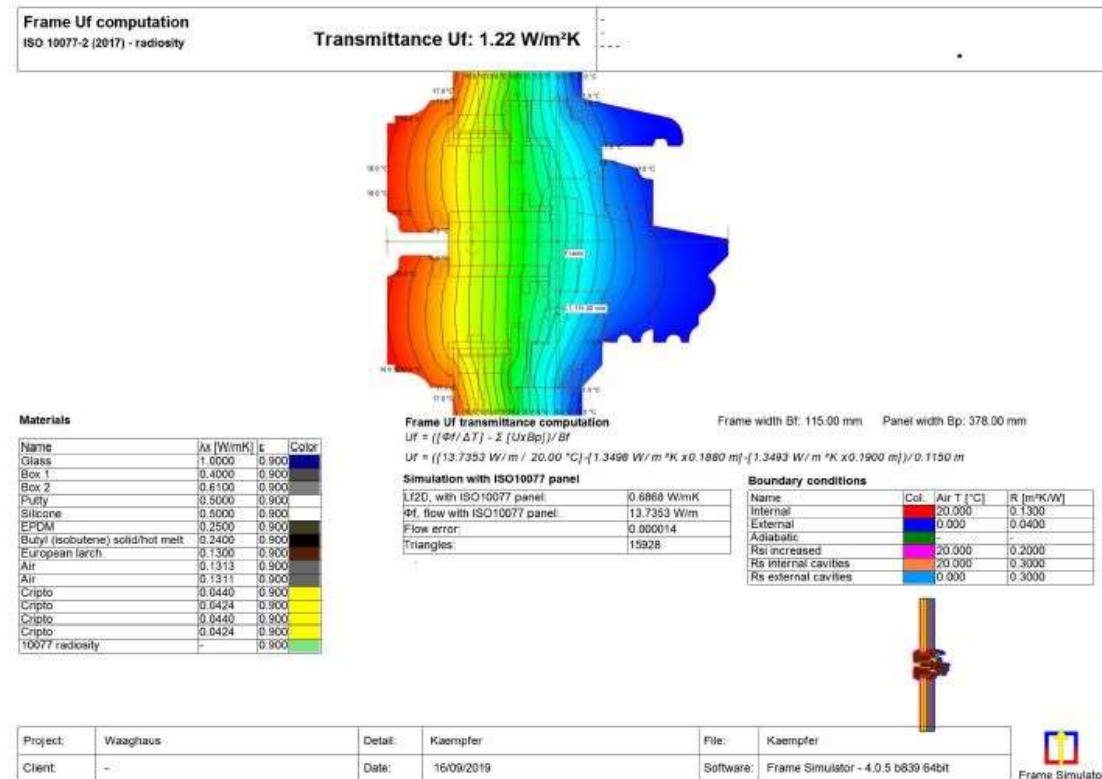
Client: -

Date: 22/09/2019

Software: Frame Simulator - 4.0.5 b839 64bit

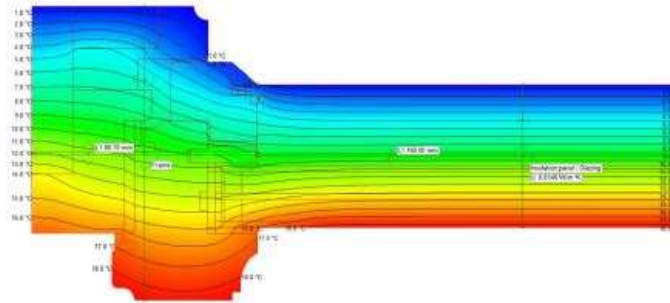


Energieeffizienter Prototyp für Verbundfenster



Frame Uf computation
ISO 10077-2 (2017) - radiosity

Transmittance Uf: 1.08 W/m²K



Materials

Name	$\lambda_{\text{c}} [\text{W/mK}]$	ϵ	Color
Glass	1.0500	0.900	
European larch	0.1300	0.950	
Insulation	0.0400	0.900	
EPDM	0.2500	0.900	
Crypto	1.0009	0.900	
Crypto	1.0361	0.900	
Box 2	0.6100	0.900	
Box 1	0.4000	0.900	
Blue ₁ (isobutene) solid/hot melt	0.2400	0.900	
Puffy	0.5000	0.900	
Air	1.0816	0.900	
10077 radiosity	-	0.900	

Frame Uf transmittance computation

Frame width Bf: 80.70 mm Panel width Bp: 190.00 mm

$$U_f = (\{ \Phi / \Delta T \} - \sum \{ U_x B_p \}) / B_f$$

$$U_f = [(7.3035 \text{ W/m} \cdot ^\circ\text{C}) - (1.3507 \text{ W/m} \cdot ^\circ\text{K} \times 0.1600 \text{ m})] \cdot (-x - f) / 0.0807 \text{ m}$$

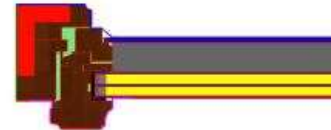
Simulation with ISO10077 panel Boundary cond

Simulation with ISO10077 panel

L/2D, with ISO10077 panel:	0.3652 W/mK
Φ , flow with ISO10077 panel:	7.3035 W/m
Flow error:	0.000027
Triangles:	14757

Boundary conditions

Name	Col.	Air T [°C]	R [m²K/W]
Internal		20.000	0.1300
External		0.000	0.0400
Adiabatic			
Rsi increased		20.000	0.2000



Project:	Waaghaus	Detail:	Rahmen 1,7,0	File:	Rahmen 1,7,0
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b639 64bit

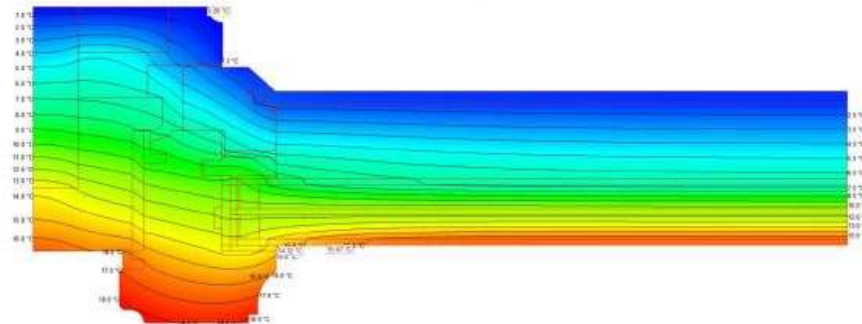


Frame Simulator

ψ and condensation computation
ISO 10077-2 (2017) - radiosity

Linear transmittance ψ : 0.021 W/mK

Superficial condensation: 0 mm



ψ computation

$$\psi = \{ \Phi \psi / \Delta T \} - \{ U f \times B f \} - \Sigma \{ U g \times B g \}$$

$$\psi = [7.3035 \text{ W/m} / 20.00 \text{ }^{\circ}\text{C}] - [1.0831 \text{ W/m}^2\text{K}^0.0807 \text{ m}] - [1.3507 \text{ W/m}^2\text{K}^0.1000 \text{ m}] - [-.]$$

Simulation with elation	Boundary conditions
$\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$ at $x = 0$ and $x = 1$ $\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$ at $y = 0$ and $y = 1$ $\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$ at $z = 0$ and $z = 1$	$\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$ at $x = 0$ and $x = 1$ $\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$ at $y = 0$ and $y = 1$ $\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = \tau_{xy} = \tau_{yz} = \tau_{zx} = 0$ at $z = 0$ and $z = 1$

Simulation with glazing

Lq2D, with glazing:	0.3652 W/mK
Φ_{gl} , flow with glazing:	7.3035 W/m
Flow error:	0.000027
Triangles:	14757

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	65.0
1	External		0.000	0.0400	65.0
2	Adiabatic		-	-	65.0
3	Soil increased		20.000	0.5000	65.0

Materials

Name	λx [W/mK]	ϵ	Color
Glass	1.0000	0.900	
European larch	0.1300	0.900	
Insulation	0.0400	0.900	
EPDM	0.2500	0.900	
Cripto	1.0000	0.900	
Cripto	1.0361	0.900	
Box 2	0.6100	0.900	
Box 1	0.4000	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	

Name	λ_x [W/mK]	ϵ	Color
Putty	0.5000	0.900	
Air	1.0816	0.900	
10077 radiosity	-	0.900	

Glazing transmittance $U_g = 1.35 \text{ W/m}^2\text{K}$

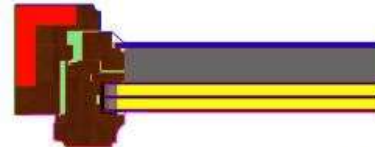
Frame transmittance $U_f=1.08 \text{ W/m}^2\text{K}$

Glazing size Bg: 190 mm

Frame size Bf: 81 mm

Boundary temperatures

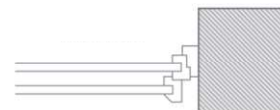
Name	L [mm]	Min T [°C]	Max T [°C]	Av. T [°C]	Q [W/m]
Internal	227.43	15.469	18.360	16.743	5.6980
External	291.83	0.261	1.637	1.001	-7.3034
Adiabatic	131.98	0.397	16.767	8.239	-0.0007
Rsi increased	87.31	14.322	18.180	16.322	1.6056

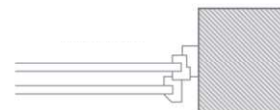
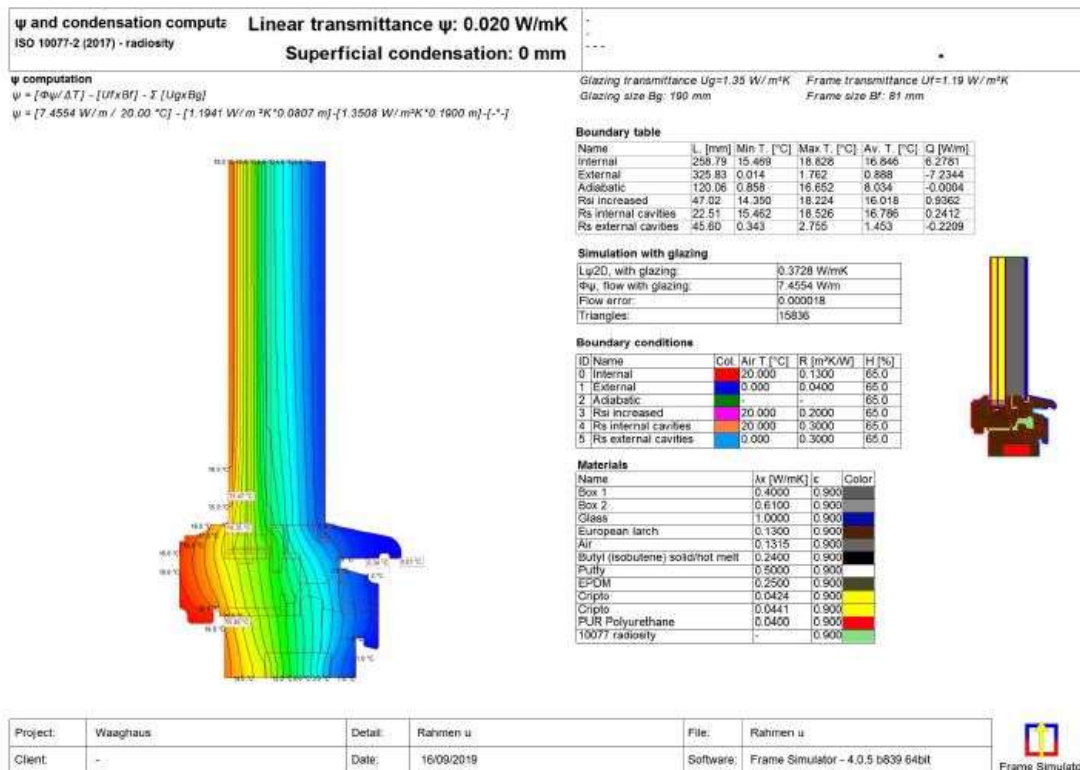
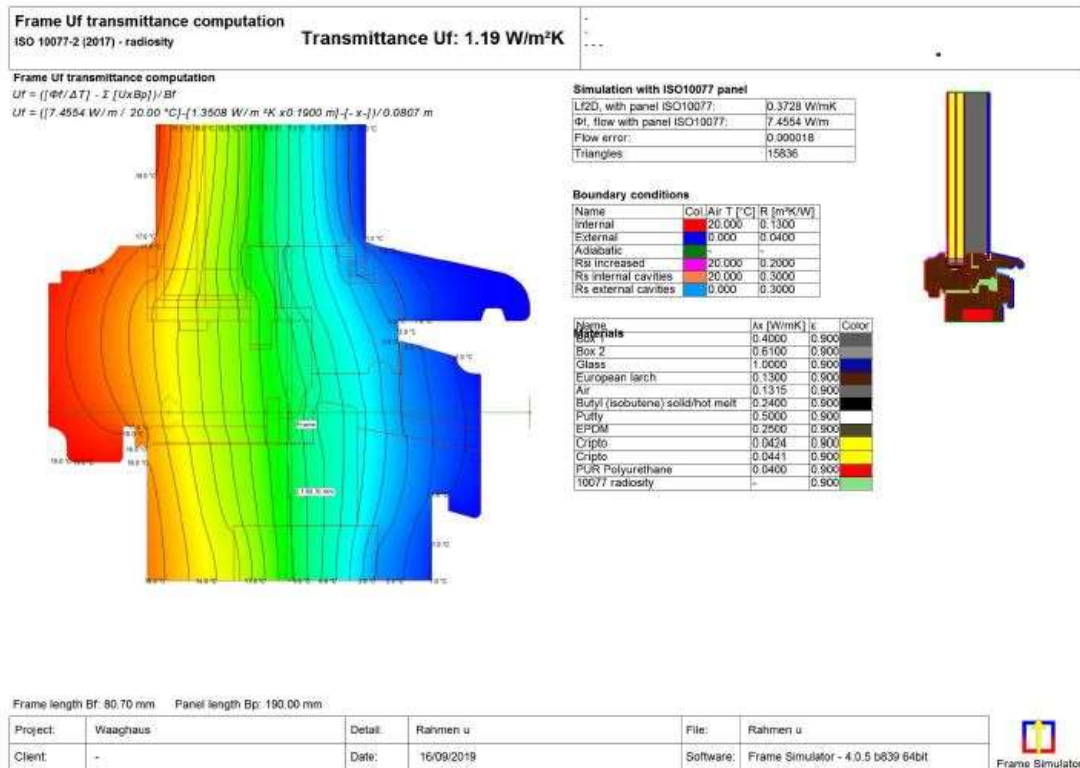


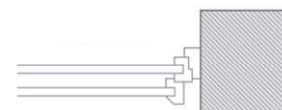
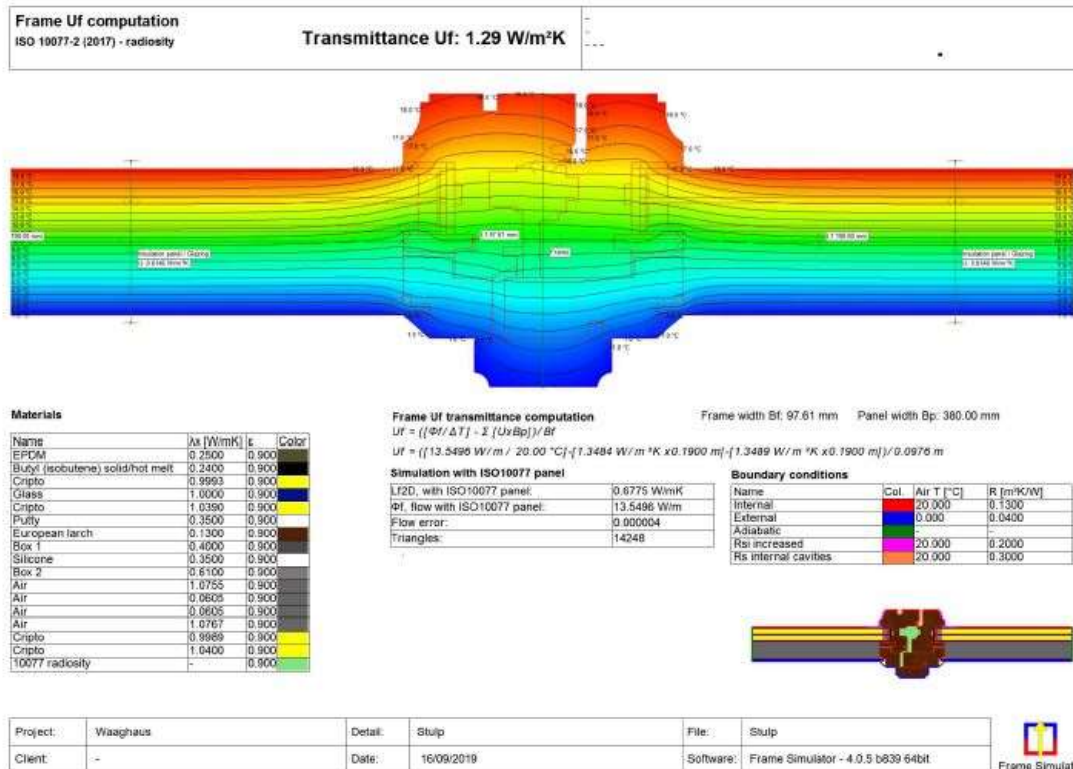
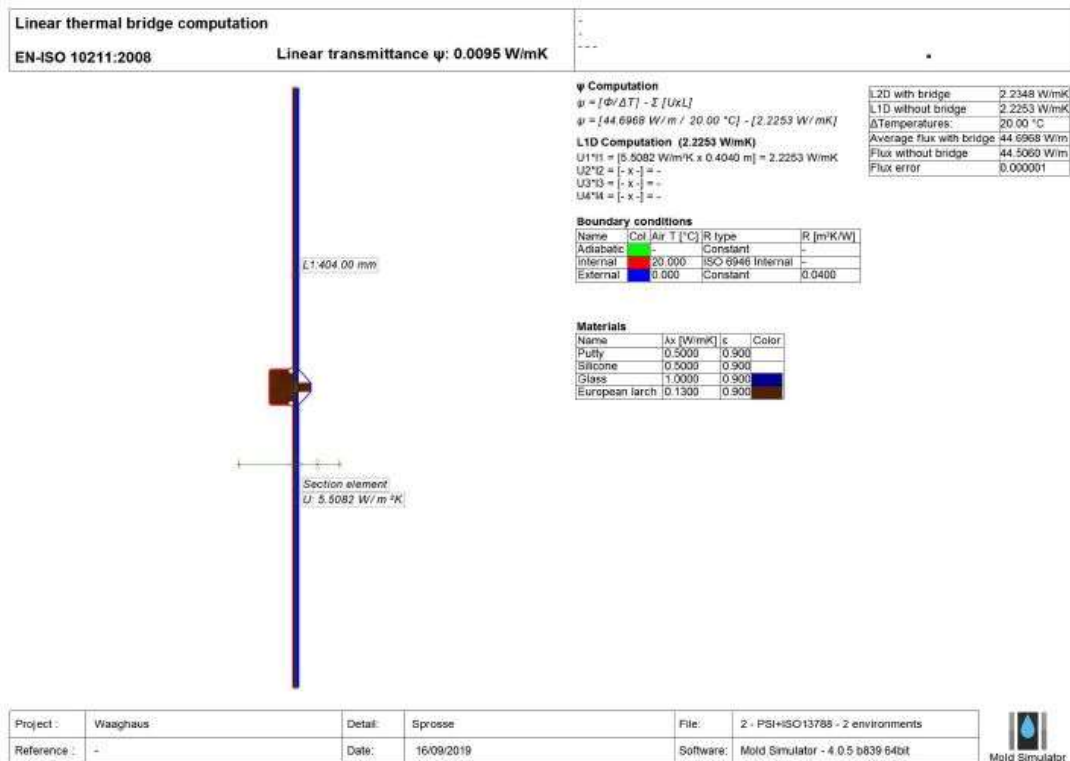
Project:	Waaghaus	Detail:	Rahmen 1,7,0	File:	Rahmen 1,7,0
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit



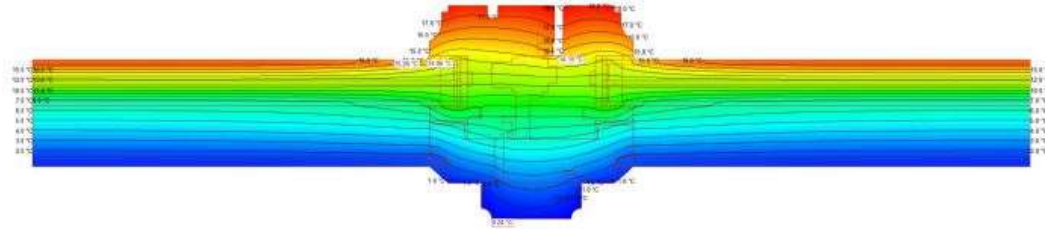
Frame Simulator







ψ and condensation computation
 ISO 10077-2 (2017) - radiosity
 Linear transmittance ψ: 0.039 W/mK
 Superficial condensation: 0 mm



ψ computation

$$\psi = [\Phi \psi / \Delta T] - [U_f \times B_f] - \Sigma [U_g \times B_g]$$

$$\psi = [13.5496 \text{ W/m}^2 / 20.00 \text{ °C}] - [1.2929 \text{ W/m}^2 \text{K} \times 0.0076 \text{ m}] - [1.3484 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}] - [1.3483 \text{ W/m}^2 \text{K} \times 0.1900 \text{ m}]$$

$$\text{Glazing transmittance } U_g = 1.35 \text{ W/m}^2 \text{K}$$

$$\text{Frame transmittance } U_f = 1.29 \text{ W/m}^2 \text{K}$$

$$\text{Glazing size } B_g = 380 \text{ mm}$$

$$\text{Frame size } B_f = 98 \text{ mm}$$

Simulation with glazing

Lq2D, with glazing:	0.6775 W/mK
ψ _{gl} , flow with glazing:	13.5496 W/m
Flow error:	0.000004
Triangles:	14248

Boundary conditions

ID	Name	Col.	Air T [°C]	R [m²K/W]	H [%]
0	Internal		20.000	0.1300	85.0
1	External		0.000	0.0400	85.0
2	Adiabatic				85.0
3	Rsi increased		20.000	0.2000	65.0
4	Rs internal cavities		20.000	0.3000	65.0

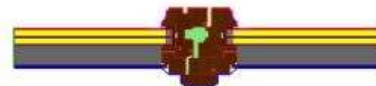
Boundary temperatures

Name	L [mm]	Min T [°C]	Max T [°C]	Avg T [°C]	Q [W/m]
Internal	415.11	15.283	18.220	16.627	10.7895
External	513.80	0.244	1.519	1.055	-13.5496
Adiabatic	101.99	1.098	16.519	6.928	0.0000
Rsi increased	95.60	14.063	18.151	15.834	1.9914
Rs internal cavities	59.67	14.191	18.220	16.604	0.7887

Materials

Name	λx [W/mK]	ε	Color
EPDM	0.2500	0.900	
Butyl (isobutene) solid/hot melt	0.2400	0.900	
Cripto	0.9999	0.900	
Glass	1.0000	0.900	
Cripto	1.0390	0.900	
Putty	0.3900	0.900	
European larch	0.1300	0.900	
Box 1	0.4000	0.900	
Silicone	0.3500	0.900	

Name	λx [W/mK]	ε	Color
Box 2	0.8100	0.900	
Air	1.0755	0.900	
Air	0.0605	0.900	
Air	0.0605	0.900	
Air	1.0767	0.900	
Cripto	0.9999	0.900	
Cripto	1.0400	0.900	
10077 radiosity	-	0.900	



Project:	Waaghaus	Detail:	Stulp	File:	Stulp
Client:	-	Date:	16/09/2019	Software:	Frame Simulator - 4.0.5 b839 64bit

